FULLER ENGINEERING & LAND SURVEYING, LLC

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Information prepared for:

WESTERN GROUP, LLC

#245 Route 32 Montville, CT &

Town of Montville
Department of Public Works / Engineering Department

Project Name: Wilton's Way Proposed Residential Development



ENGINEERING REPORT

Documentation

Dated: January 25, 2022 Revised: March 8, 2022

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OWNER/APPLICANT: PROJECT LOCATION: WESTERN GROUP, LLC

WILTONS WAY #245 Route 32,

Montville, Connecticut

DRAINAGE STUDY

<u>INTRODUCTION</u>

The purpose of this study is to outline the storm water analysis for the proposed development at #245 Norwich-New London Road Town of Montville, Route 32 Uncasville, CT. The storm water management plan is based on a hydrologic analysis of pre-development and postdevelopment conditions using a Type III-24 Hour, for 25 -year frequency storms. The peak flow rate and the increase in runoff for up to the 50-year storm frequency is being compared in this study. The hydrological analysis is conducted within the area of the property as bounded by the property lines shown on the plan only.

Western Group, LLC is proposing to construct two multi-level residential condominium buildings, basements, new driveways and miscellaneous landscaping at 245 Norwich-New London Road, Route 32 Montville, CT. The proposed development is located on the east side of State Route 32 travelling northbound. Refer to the plan titled "Wilton's Way" 22 Unit Condominium Development dated January 4, 2022, Revised 3/8/2022 prepared for Western Group, LLC prepared by Fuller Engineering & Land Surveying, LLC for the extent of the proposed development.

The proposed development will increase the amount of impervious area on the site, and will therefore increase the runoff rain water leaving the site. The analysis did not consider back-toback storms.

PRE-DEVELOPMENT CONDITIONS

The site considered in this study is the entire area of the property which is located in the C-1 District, which is a Commercial Zone, although the proposed development will be strictly residential use. The total area (79,607 s.f.) (1.828 acre) currently is composed of mainly pervious surfaces will little impervious land surface.

The runoff from this area sheet flows towards the East at the low point on the property (considered as POC "A") (outfall 1L in Hydrocad). The peak flow towards POC "A" for a Type III-24 Hour, for 25 -year frequency storms is 4.76 cfs.

> FULLER ENGINEERING & LAND SURVEYING, LLC 525 JOHN STREET 2ND FLOOR BRIDGEPORT, CONNECTICUT 06604 PHONE (203)333-9465; FAX (203)336-1769

PROPOSED POST-DEVELOPMENT CONDITIONS

The proposed developments on said parcel with area of (79,607 s.f.) will be two (2) multi story residential condominium buildings, common drive and independent driveway/parking and miscellaneous landscaping. The proposed development will increase the impervious surface by 42,965 s.f. within the watershed encompassing POC "A". Stormwater runoff from the proposed building and basement driveway will be directed to the inlet structure which is connected to 60 units 4' x 8' x 4' Concrete Galleys in 2 groups, first set of 28 embedded in 58' x 18.6' x 5.17' gravel bed, and a second set of 32 embedded in 66' x 18.6' x 5.17' gravel bed to help treat water quality and attenuate the storm water runoff going to the control structure at the back of the retaining wall before discharging to 12" RCP to the 40' long ADS-N12 15"Ø slotted pipe encased in 42'x 3.5'x 3.17' gravel bed Level Spreader moving towards POC "A" (outfall 1L in Hydrocad). Storm water runoff from the driveways and common drive will sheet flow into common drive catch basin distributing the stormwater along the edge of the common drive in a storm sewer system. Roof drains will be directly connected underground to the concrete galley system. The overflow of the concrete galley system will be directed to a control structure which will discharge the water into a energy dissipating level spreader. The peak flow towards POC "A" for a Type III-24 Hour, for 25 -year frequency storm, post development is 4.52 cfs. which is less than the pre development conditions.

DESIGN METHODOLOGY

The site consists of a Hydrological Soil Group (HSG) rating C (refer to Appendix B) which is used in the analysis. The following CN values are used; (a) 98 for impervious surfaces; (b) 81 for HSG C, 30% imp. 1/3 acre residential; (c) 65 for HSG C, 50-75% grass cover, good condition.

HydroCAD Version 10.0 was utilized to evaluate the runoff volume and peak discharge rates of the pre and post-development conditions. The design storm frequencies considered are the 2-year, 5-year, 10-year, 25-year, and 50-year storm frequencies. They were used in the analysis with the following 24-hour rainfall total; 2-year, 3.46 inches; 5-year, 4.36 in.; 10-year, 5.12 inches; 25-year, 6.15 inches; and 50-year, 6.93 inches. The peak flow towards POC "A" at the wooded border is less than the pre-development runoff peak flows as shown in Table 1.

TABLE 1 – Peak Flows in cfs/Volume in C.F.

STORM EVENT	LINK/POC		FLOW/VOLUME	EXISTING	PROPOSED	Δ	Δ (%)
2 Year Storm	LINK 1	(A)	q (ft ³ /s)	1.61	0.18	-1.43	-88.8
			v (ft ³)	7613	1187	-6426	-84.4
5 Year Storm	LINK 1	(A)	q (ft ³ /s)	2.6	0.84	-1.76	-67.7
			v (ft³)	11831	2936	-8895	-75.2
10 Year Storm	LINK 1	(A)	q (ft ³ /s)	3.49	1.72	-1.77	-50.7
			v (ft³)	15694	6274	-9420	-60.0
25 Year Storm	LINK 1	/^\	q (ft ³ /s)	4.76	4.52	-0.24	-5.0
		(A)	v (ft ³)	21240	11149	-10091	-47.5
50 Year Storm	LINK 1	(A)	q (ft³/s)	5.75	6.17	0.42	7.3
			v (ft ³)	25616	15101	-10515	-41.0

Based on the tabulated results above, the peak flows and the run off volume of the post-development condition are less than the pre-development conditions.

SOIL EROSION AND SEDIMENTATION CONTROL

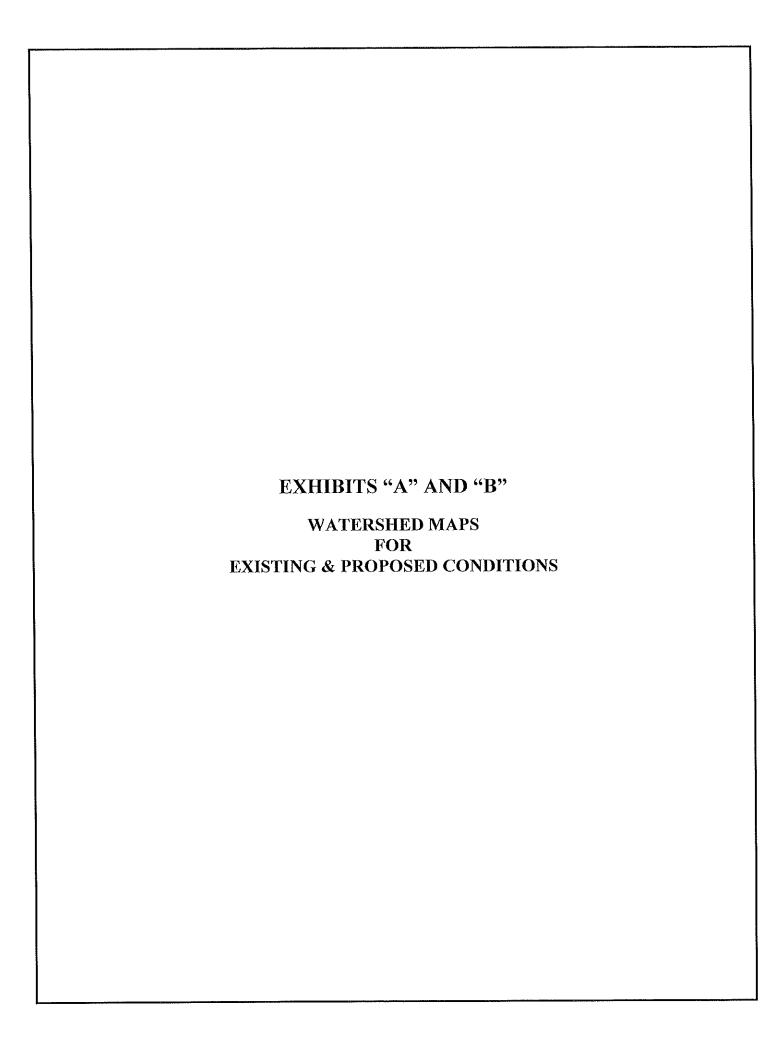
For temporary condition or during construction a silt fence shall be provided along the property lines. Anti-tracking aprons shall be provided at all access routes from the site to the public road. A temporary diversion berm with stone check dams @ 50 ft o.c. shall be maintained and relocated as required during construction. All planting areas shall be protected with slope stabilization measures.

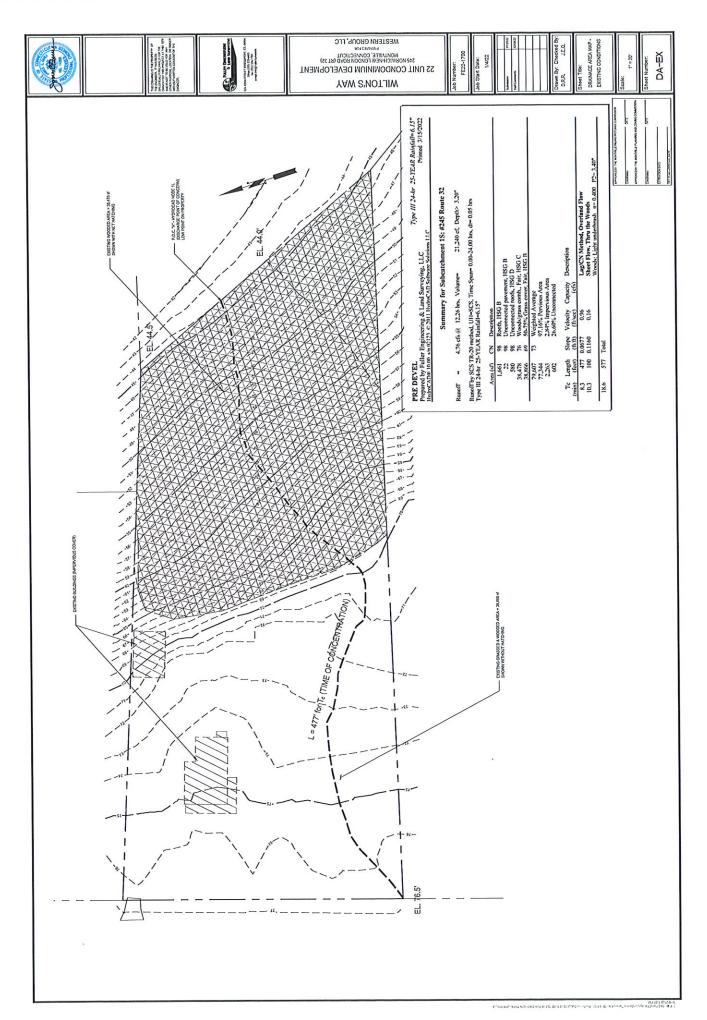
For permanent condition, all embankments, after being stabilized, shall be sodded. Newly planted areas shall be covered with straw or erosion control blankets.

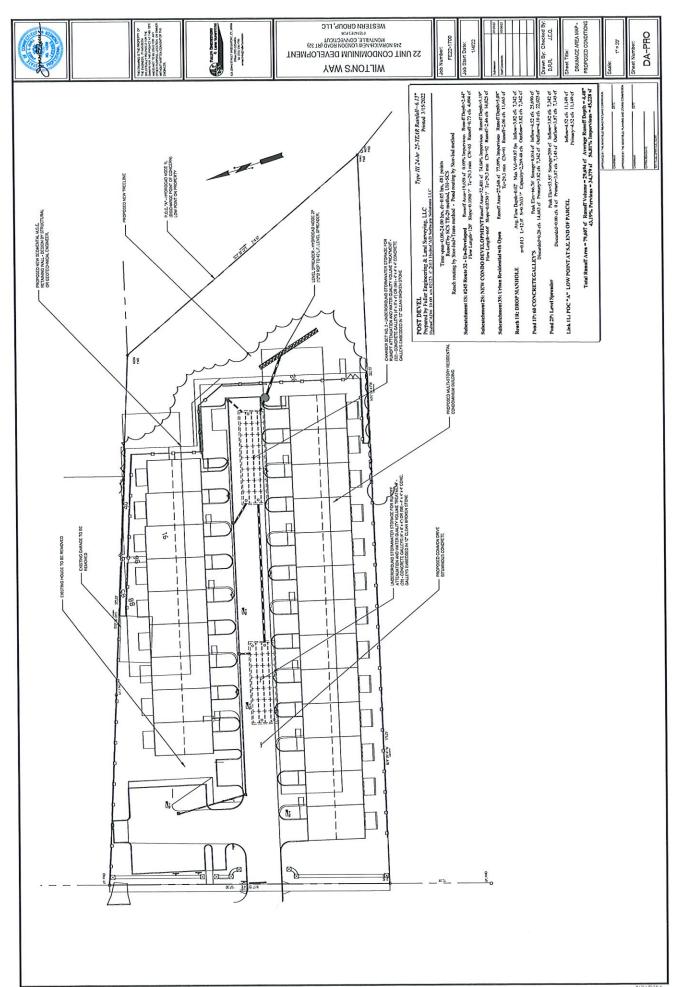
CONCLUSION

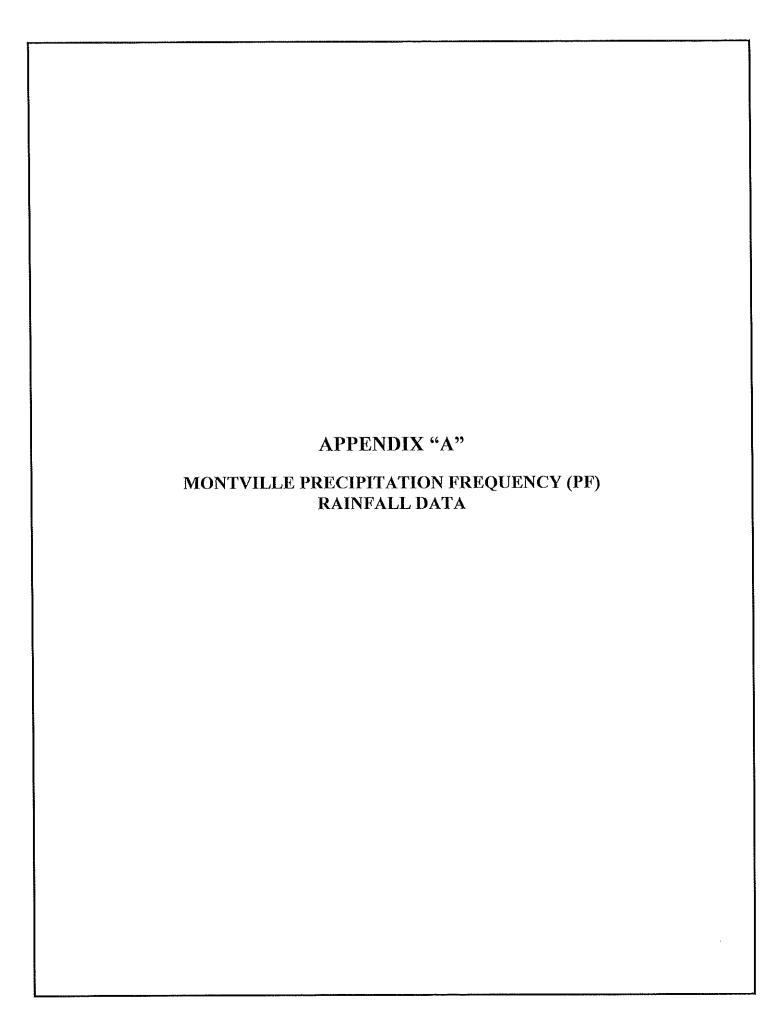
The proposed development will increase the impervious coverage on the site thus increase the volume and peak flow rate of runoff generated during a storm event. However, to address the water quality volume and peak flow issues, a subsurface detention/retention system will be installed to treat and attenuate the storm water runoff. The proposed development will not increase the peak flow rate to the POC for up to the 25-year frequency storm.

Since the proposed development incorporates pre-treatment and attenuation of runoff to the maximum extent practical, if the proposed development is constructed as depicted on the proposed development plans, then there will be no adverse impacts to adjoining properties and/or street drainage.



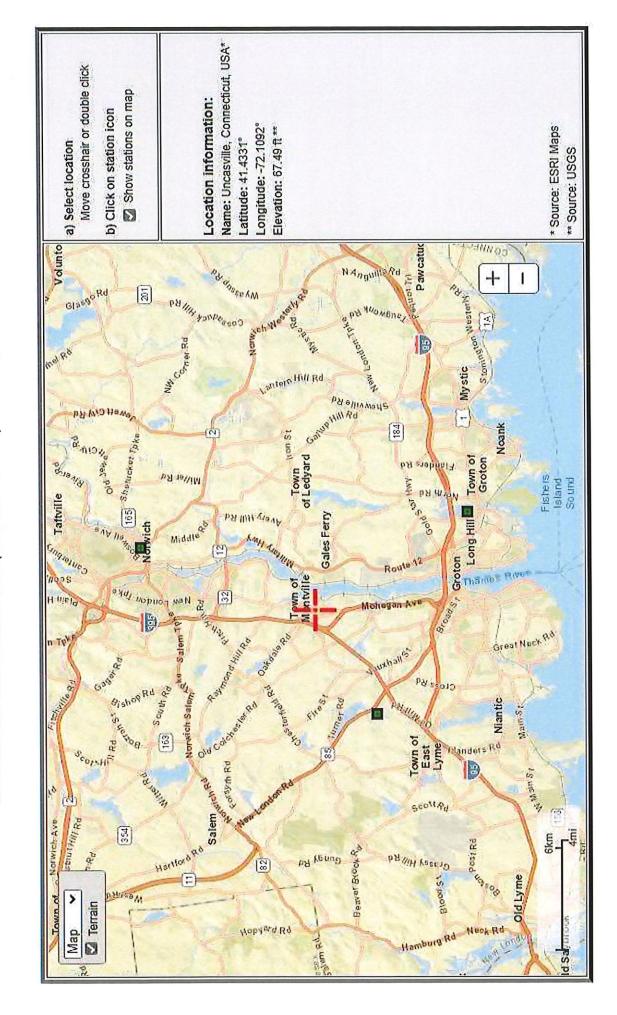






NOAA ATLAS 14 POINT PRECIPITATION FREQUENCY ESTIMATES: CT

#245 Norwich New London Road (CT State RTE. 32) Montville, CT





NOAA Atlas 14, Volume 10, Version 3 Location name: Uncasville, Connecticut, USA* Latitude: 41.4331°, Longitude: -72.1092° Elevation: 67.49 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹								ches) ¹	
Duration	Average recurrence interval (years)									
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.340 (0.266-0.427)	0.406 (0.317-0.510)	0.514 (0.400-0.648)	0.604 (0.467-0.763)	0.727 (0.545-0.952)	0.820 (0.601-1.09)	0.918 (0.654-1.26)	1.03 (0.693-1.43)	1.19 (0.770-1.70)	1.32 (0.835-1.91)
10-min	0.482 (0.377-0.605)	0.576 (0.449-0.723)	0.729 (0.567-0.918)	0.856 (0.662-1.08)	1.03 (0.772-1.35)	1.16 (0.853-1.55)	1.30 (0.926-1.78)	1.46 (0.982-2.02)	1.68 (1.09-2.40)	1.87 (1.18-2.71)
15-min	0.567 (0.443-0.712)	0.677 (0.529-0.851)	0.857 (0.667-1.08)	1.01 (0.779-1.27)	1.21 (0.908-1.59)	1.37 (1.00-1.82)	1.53 (1.09-2.10)	1.71 (1.16-2.38)	1.98 (1.28-2.83)	2.20 (1.39-3.19)
30-min	0.803 (0.627-1.01)	0.958 (0.747-1.20)	1.21 (0.942-1.53)	1.42 (1.10-1.80)	1.71 (1.28-2.24)	1.93 (1.41-2.57)	2.16 (1.54-2.96)	2.42 (1.63-3.36)	2.79 (1.81-3.99)	3.10 (1.96-4.50)
60-min	1.04 (0.811-1.30)	1.24 (0.966-1.56)	1.57 (1.22-1.97)	1.84 (1.42-2.32)	2.21 (1.66-2.89)	2.49 (1.83-3.32)	2.79 (1.99-3.82)	3.12 (2.10-4.34)	3.61 (2.34-5.15)	4.01 (2.53-5.81)
2-hr	1.36 (1.08-1.70)	1.63 (1.28-2.03)	2.05 (1.61-2.57)	2.41 (1.88-3.02)	2.90 (2.19-3.77)	3.26 (2.41-4.31)	3.65 (2.62-4.97)	4.10 (2.78-5.65)	4.75 (3.09-6.72)	5.28 (3.36-7.59)
3-hr	1.58 (1.25-1.96)	1.89 (1.49-2.34)	2.38 (1.88-2.96)	2.79 (2.19-3.48)	3.35 (2.54-4.34)	3.78 (2.81-4.97)	4.22 (3.05-5.73)	4.74 (3.22-6.50)	5.49 (3.59-7.74)	6.12 (3.90-8.75)
6-hr	2.01 (1.60-2.47)	2.39 (1.90-2.94)	3.00 (2.39-3.70)	3.51 (2.78-4.35)	4.22 (3.22-5.41)	4.75 (3.55-6.19)	5.30 (3.85-7.13)	5.95 (4.07-8.08)	6.89 (4.52-9.61)	7.67 (4.91-10.9)
12-hr	2.48 (2.00-3.02)	2.94 (2.36-3.59)	3.69 (2.96-4.52)	4.31 (3.44-5.30)	5.17 (3.98-6.58)	5.81 (4.38-7.52)	6.49 (4.74-8.65)	7.28 (5.00-9.80)	8.42 (5.55-11.6)	9.37 (6.02-13.2)
24-hr	2.90 (2.36-3.51)	3.46 (2.80-4.18)	4.36 (3.53-5.30)	5.12 (4.11-6.24)	6.15 (4.77-7.77)	6.93 (5.26-8.89)	7.75 (5.71-10.3)	8.71 (6.02-11.6)	10.1 (6.71-13.9)	11.3 (7.31-15.7)
2-day	3.25 (2.66-3.89)	3.91 (3.20-4.69)	4.99 (4.06-6.00)	5.88 (4.77-7.11)	7.12 (5.57-8.92)	8.03 (6.15-10.3)	9.02 (6.71-11.9)	10.2 (7.09-13.5)	12.0 (7.97-16.3)	13.5 (8.75-18.6)
3-day	3.52 (2.90-4.20)	4.23 (3.48-5.06)	5.40 (4.43-6.47)	6.37 (5.19-7.66)	7.70 (6.06-9.62)	8.69 (6.69-11.0)	9.76 (7.29-12.8)	11.0 (7.70-14.5)	13.0 (8.66-17.5)	14.6 (9.51-20.0)
4-day	3.78 (3.12-4.50)	4.53 (3.74-5.39)	5.75 (4.73-6.87)	6.77 (5.53-8.12)	8.17 (6.45-10.2)	9.21 (7.11-11.7)	10.3 (7.73-13.5)	11.7 (8.15-15.3)	13.7 (9.16-18.4)	15.4 (10.0-21.0)
7-day	4.50 (3.75-5.33)	5.32 (4.43-6.30)	6.66 (5.52-7.90)	7.77 (6.40-9.26)	9.30 (7.38-11.5)	10.4 (8.10-13.1)	11.7 (8.75-15.1)	13.1 (9.20-17.0)	15.2 (10.2-20.3)	17.0 (11.1-23.1)
10-day	5.22 (4.37-6.15)	6.08 (5.08-7.16)	7.48 (6.22-8.83)	8.64 (7.14-10.2)	10.2 (8.16-12.5)	11.4 (8.90-14.2)	12.7 (9.55-16.3)	14.2 (9.99-18.4)	16.3 (11.0-21.6)	18.0 (11.8-24.3)
20-day	7.42 (6.26-8.66)	8.33 (7.03-9.74)	9.83 (8.25-11.5)	11.1 (9.23-13.0)	12.8 (10.2-15.4)	14.1 (11.0-17.2)	15.4 (11.5-19.3)	16.8 (11.9-21.5)	18.7 (12.7-24.6)	20.1 (13.3-26.9)
30-day	9.25 (7.85-10.7)	10.2 (8.65-11.9)	11.8 (9.92-13.7)	13.0 (10.9-15.3)	14.8 (11.9-17.7)	16.2 (12.7-19.6)	17.5 (13.1-21.7)	18.9 (13.5-24.0)	20.5 (14.0-26.8)	21.7 (14.4-28.9)
45-day	11.5 (9.82-13.3)	12.5 (10.7-14.5)	14.1 (12.0-16.4)	15.5 (13.1-18.0)	17.4 (14.0-20.7)	18.9 (14.8-22.7)	20.3 (15.2-24.8)	21.5 (15.4-27.2)	23.0 (15.7-29.9)	24.0 (15.9-31.7)
60-day	13.4 (11.5-15.4)	14.4 (12.3-16.6)	16.2 (13.8-18.7)	17.6 (14.9-20.4)	19.6 (15.8-23.1)	21.1 (16.6-25.3)	22.6 (16.9-27.5)	23.8 (17.1-30.0)	25.2 (17.3-32.6)	26.1 (17.4-34.3)

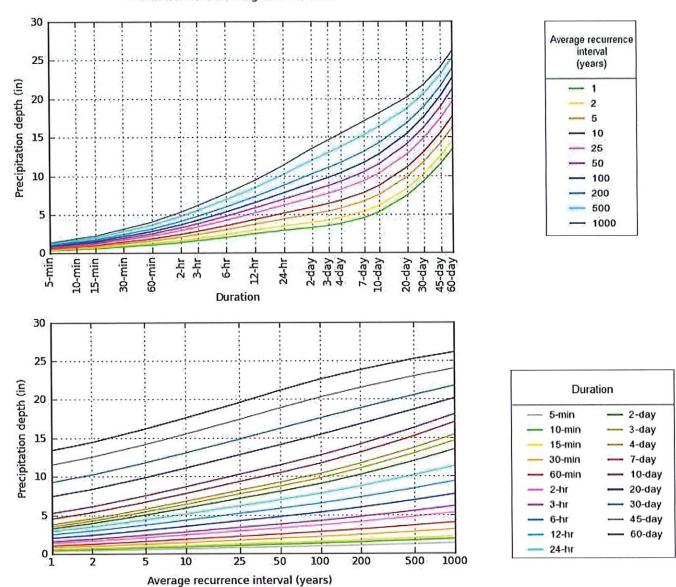
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PDS-based depth-duration-frequency (DDF) curves Latitude: 41.4331°, Longitude: -72.1092°



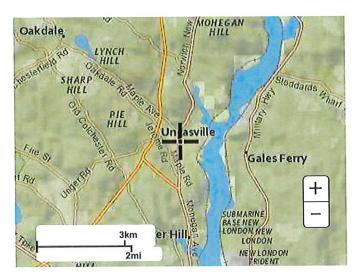
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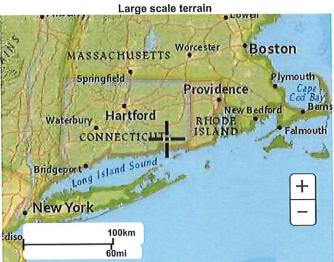
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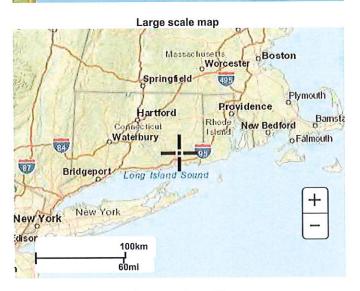
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Maps & aerials

Small scale terrain







Large scale aerial



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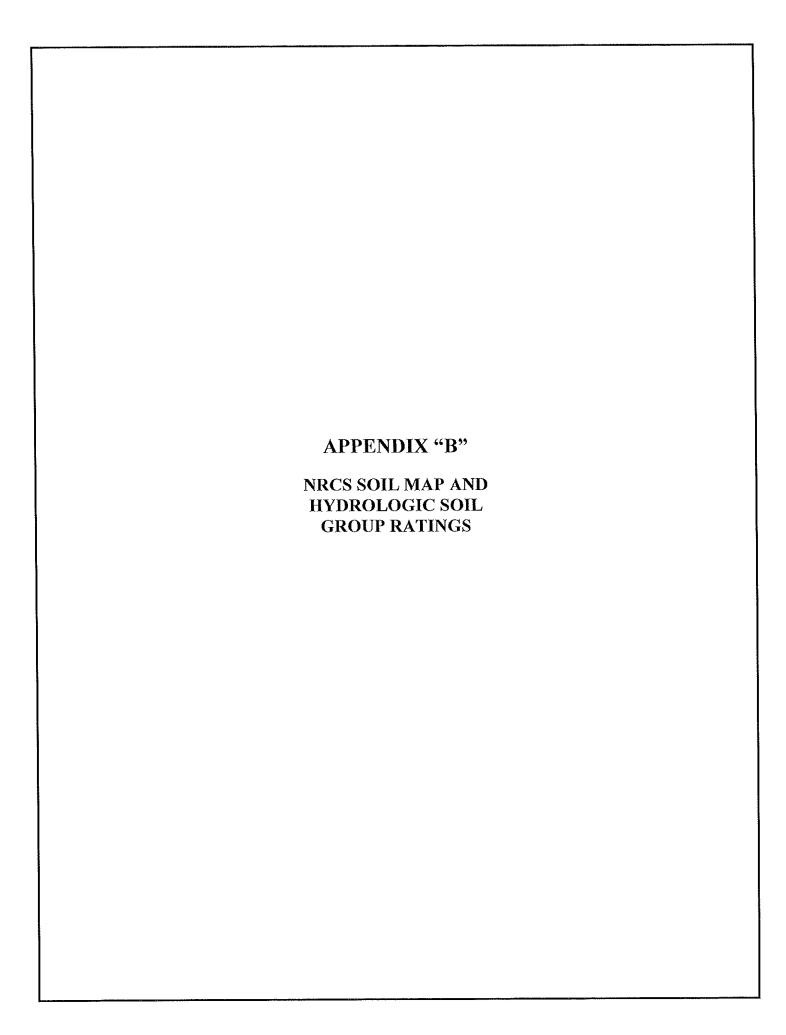
National Water Center

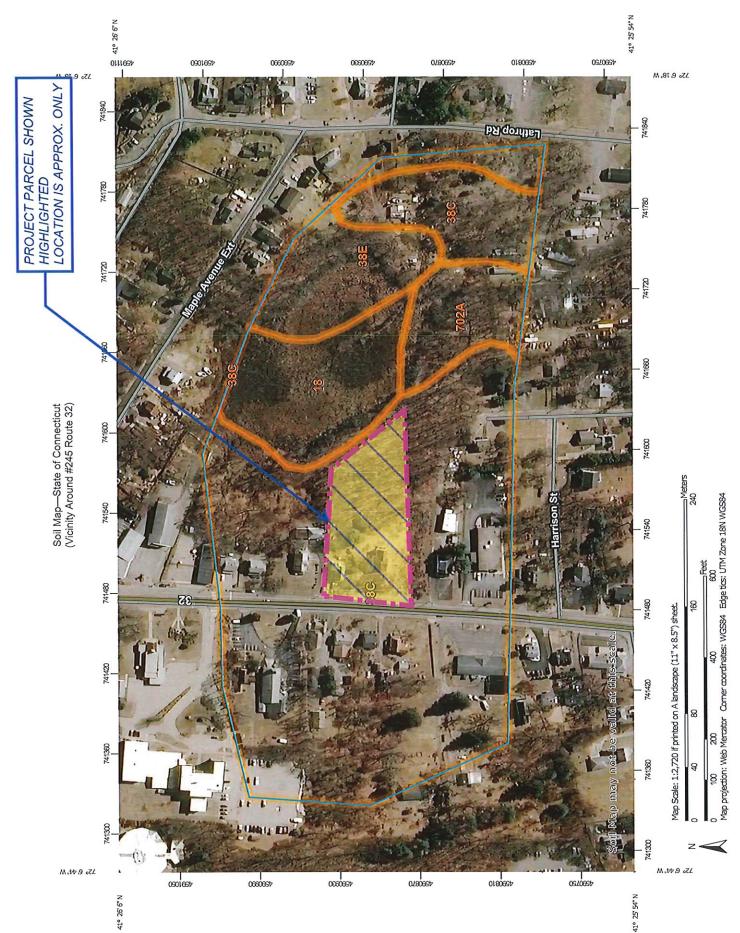
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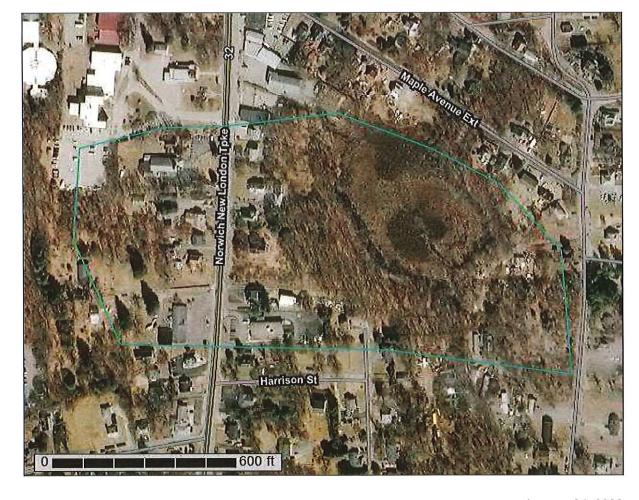




NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for State of Connecticut



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

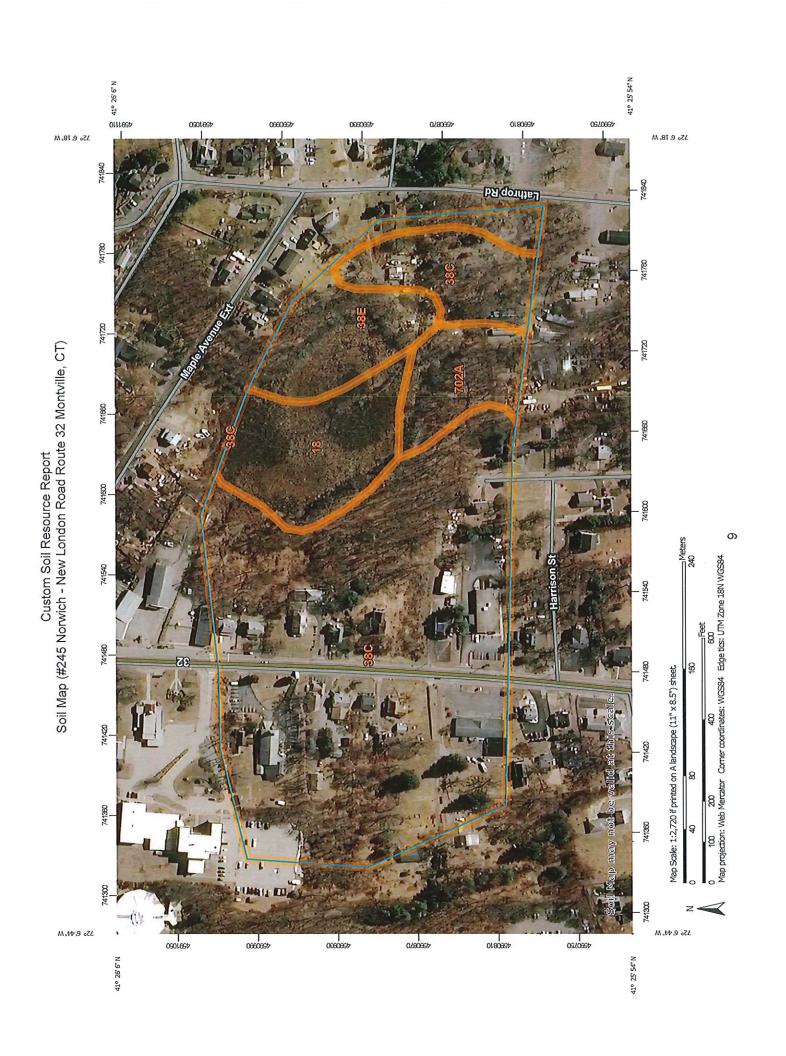
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



This product is generated from the USDA-NRCS certified data as distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator Date(s) aerial images were photographed: Mar 20, 2019-Mar contrasting soils that could have been shown at a more detailed The orthophoto or other base map on which the soil lines were misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of Enlargement of maps beyond the scale of mapping can cause compiled and digitized probably differs from the background projection, which preserves direction and shape but distorts Soil map units are labeled (as space allows) for map scales imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. Albers equal-area conic projection, should be used if more Source of Map: Natural Resources Conservation Service The soil surveys that comprise your AOI were mapped at Please rely on the bar scale on each map sheet for map accurate calculations of distance or area are required. Coordinate System: Web Mercator (EPSG:3857) MAP INFORMATION Warning: Soil Map may not be valid at this scale. Survey Area Data: Version 21, Sep 7, 2021 State of Connecticut of the version date(s) listed below. Web Soil Survey URL: 1:50,000 or larger. Soil Survey Area: measurements. 27, 2019 1:12,000. scale. Special Line Features Streams and Canals Interstate Highways Aerial Photography Very Stony Spot Major Roads Local Roads Stony Spot **US Routes** Spoil Area Wet Spot Other Rails Nater Features **Fransportation** Background MAP LEGEND 8 0 ‡ Soil Map Unit Polygons Severely Eroded Spot Area of Interest (AOI) Miscellaneous Water Soil Map Unit Points Soil Map Unit Lines Closed Depression Marsh or swamp Perennial Water Mine or Quarry Rock Outcrop Special Point Features **Gravelly Spot** Saline Spot Sandy Spot Slide or Slip Sodic Spot Borrow Pit Lava Flow Clay Spot **Gravel Pit** Area of Interest (AOI) Sinkhole Blowout Landfill 9 ፠ \Diamond X

Map Unit Legend (#245 Norwich - New London Road Route 32 Montville, CT)

	HEADING SAUGENA DE LA COMPANION DE LA COMPANIO				
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI		
18	Catden and Freetown soils, 0 to 2 percent slopes	2.8	11.7%		
38C	Hinckley loamy sand, 3 to 15 percent slopes	17.0	70.7%		
38E	Hinckley loamy sand, 15 to 45 percent slopes	2.7	11.1%		
702A	Tisbury silt loam, 0 to 3 percent slopes	1.6	6.5%		
Totals for Area of Interest	<u> </u>	24.0	100.0%		

Map Unit Descriptions (#245 Norwich - New London Road Route 32 Montville, CT)

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it

was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a soil series. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas, Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

State of Connecticut

18—Catden and Freetown soils, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2t2r2

Elevation: 0 to 1,390 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Catden and similar soils: 45 percent Freetown and similar soils: 35 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Catden

Setting

Landform: Depressions, kettles, marshes, swamps, depressions, bogs, fens,

depressions

Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed herbaceous organic material and/or highly

decomposed woody organic material

Typical profile

Oa1 - 0 to 2 inches: muck Oa2 - 2 to 79 inches: muck

Properties and qualities

Slope: 0 to 2 percent

Surface area covered with cobbles, stones or boulders: 0.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: NoneRare Frequency of ponding: Frequent

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Very high (about 26.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Ecological site: F144AY042NY - Semi-Rich Organic Wetlands

Hydric soil rating: Yes

Description of Freetown

Setting

Landform: Depressions, marshes, depressions, bogs, swamps, kettles

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed organic material

Typical profile

Oe - 0 to 2 inches: mucky peat Oa - 2 to 79 inches: muck

Properties and qualities

Slope: 0 to 2 percent

Surface area covered with cobbles, stones or boulders: 0.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: NoneRare Frequency of ponding: Frequent

Available water supply, 0 to 60 inches: Very high (about 26.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Ecological site: F144AY043MA - Acidic Organic Wetlands

Hydric soil rating: Yes

Minor Components

Natchaug

Percent of map unit: 7 percent

Landform: Depressions, depressions, depressions Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Whitman

Percent of map unit: 6 percent

Landform: Drainageways, depressions

Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Timakwa

Percent of map unit: 5 percent

Landform: Depressions

Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Scarboro

Percent of map unit: 2 percent

Landform: Depressions, drainageways, outwash deltas, outwash terraces

Landform position (three-dimensional): Base slope, tread, dip

Down-slope shape: Concave

Across-slope shape: Concave, linear

Hydric soil rating: Yes

38C—Hinckley loamy sand, 3 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2svmb

Elevation: 0 to 1,290 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hinckley

Setting

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces

Landform position (two-dimensional): Summit, shoulder, backslope, footslope, toeslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest, riser, tread

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand C - 19 to 65 inches: very gravelly sand

Properties and qualities

Slope: 3 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

Minor Components

Merrimac

Percent of map unit: 5 percent

Landform: Kames, outwash plains, outwash terraces, moraines, eskers

Landform position (two-dimensional): Summit, shoulder, backslope, footslope, toeslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

Windsor

Percent of map unit: 5 percent

Landform: Moraines, eskers, kames, outwash deltas, outwash terraces, outwash plains, kame terraces

Landform position (two-dimensional): Summit, shoulder, backslope, footslope, toeslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest, riser, tread

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

Agawam

Percent of map unit: 3 percent

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces

Landform position (two-dimensional): Summit, shoulder, backslope, toeslope, footslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest, riser, tread

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

Sudbury

Percent of map unit: 2 percent

Landform: Outwash deltas, moraines, outwash plains, kame terraces, outwash terraces

Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, linear Across-slope shape: Concave, linear

Hydric soil rating: No

38E—Hinckley loamy sand, 15 to 45 percent slopes

Map Unit Setting

National map unit symbol: 2svmj

Elevation: 0 to 1,280 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hinckley

Setting

Landform: Eskers, kames, outwash deltas, outwash terraces, moraines, outwash plains, kame terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest, riser

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

Properties and qualities

Slope: 15 to 45 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

Minor Components

Windsor

Percent of map unit: 5 percent

Landform: Eskers, kames, moraines, outwash deltas, outwash terraces, outwash plains, kame terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

Merrimac

Percent of map unit: 5 percent

Landform: Outwash plains, outwash terraces, moraines, eskers, kames

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

riser

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Agawam

Percent of map unit: 3 percent

Landform: Eskers, kame terraces, outwash deltas, outwash terraces, moraines, kames, outwash plains

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

Sudbury

Percent of map unit: 2 percent

Landform: Kames, eskers, outwash deltas, outwash plains, kame terraces,

outwash terraces, moraines

Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, linear Across-slope shape: Linear, concave

Hydric soil rating: No

702A—Tisbury silt loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2y07g

Elevation: 0 to 1,260 feet

Mean annual precipitation: 43 to 54 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 140 to 185 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Tisbury and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Tisbury

Setting

Landform: Outwash terraces, deltas, outwash plains, valley trains

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-silty eolian deposits over sandy and gravelly glaciofluvial

deposits derived from granite, schist, and/or gneiss

Typical profile

Ap - 0 to 8 inches: silt loam Bw1 - 8 to 18 inches: silt loam Bw2 - 18 to 26 inches: silt loam

2C - 26 to 65 inches: extremely gravelly sand

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: 24 to 36 inches to strongly contrasting textural

stratification

Drainage class: Moderately well drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 18 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: F144AY026CT - Moist Silty Outwash

Hydric soil rating: No

Minor Components

Merrimac

Percent of map unit: 5 percent

Landform: Outwash plains, outwash terraces, moraines, eskers, kames

Landform position (two-dimensional): Summit, shoulder

Landform position (three-dimensional): Side slope, crest, tread

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Agawam

Percent of map unit: 5 percent

Landform: Kame terraces, outwash plains, outwash terraces, moraines, kames

Landform position (two-dimensional): Summit, shoulder

Landform position (three-dimensional): Side slope, crest, tread

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Ninigret

Percent of map unit: 3 percent

Landform: Kame terraces, outwash plains, moraines, kames, outwash terraces

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Convex, linear Across-slope shape: Convex, concave

Hydric soil rating: No

Raypol

Percent of map unit: 2 percent

Landform: Drainageways, depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

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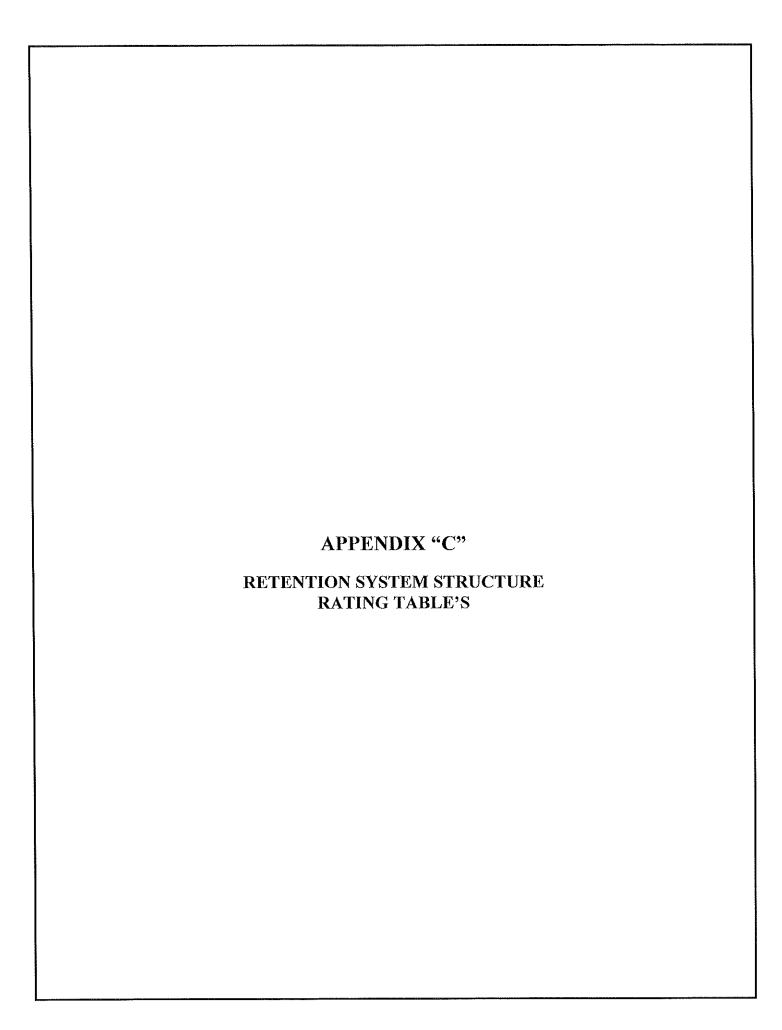
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Stage-Area-Storage for Pond 1P: 60 CONCRETE GALLEY'S

Elevation	Surface	Storage	Elevation	Surface	Storage	
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)	
57.33	2,574	0	60.51	2,574	5,527	
57.39	2,574	62	60.57	2,574	5,639	
57.45	2,574	124	60.63	2,574	5,750	
57.51	2,574	185	60.69	2,574	5,861	
57.57	2,574	247	60.75	2,574	5,973	
57.63	2,574	309	60.81	2,574	6,084	
57.69	2,574	371	60.87	2,574	6,195	
57.75	2,574	432	60.93	2,574	6,306	
57.81	2,574	494	60.99	2,574	6,417	
57.87	2,574	588	61.05	2,574	6,528	
57.93	2,574	697	61.11	2,574	6,639	
57.99	2,574	806	61.17	2,574	6,750	
58.05	2,574	916	61.23	2,574	6,861	
58.11	2,574	1,029	61.29	2,574	6,972	
58.17	2,574	1,142	61.35	2,574	7,082	
58.23	2,574	1,255	61.41	2,574	7,193	
58.29	2,574	1,369	61.47	2,574	7,212	4
58.35	2,574	1,482	61.53	2,574	7,232	
58.41	2,574	1,595	61.59	2,574	7,251	
58.47	2,574	1,708	61.65	2,574	7,270	
58.53	2,574	1,822	61.71	2,574	7,289	
58.59	2,574	1,935	61.77	2,574	7,309	
58.65	2,574	2,048	61.83	2,574	7,328	
58.71	2,574	2,161	61.89	2,574	7,390	
58.77	2,574	2,274	61.95	2,574	7,452	
58.83	2,574	2,387	62.01	2,574	7,513	
58.89	2,574	2,500	62.07	2,574	7,575	
58.95	2,574	2,612	62.13	2,574	7,637	
59.01	2,574	2,725	62.19	2,574	7,699	
59.07	2,574	2,838	62.25	2,574	7,761	
59.13	2,574	2,950	62.31	2,574	7,822	
59.19	2,574	3,063	62.37	2,574	7,884	
59.25	2,574	3,176	62.43	2,574	7,946	
59.31	2,574	3,288	62.49	2,574	8,008	
59.37	2,574	3,400	62.55	2,574	8,014	
59.43	2,574	3,513	62.61	2,574	8,014	
59.49	2,574	3,625	62.67	2,574	8,014	
59.55	2,574	3,738	62.73	2,574	8,014	
59.61	2,574	3,850	62.79	2,574	8,014	
59.67	2,574	3,962	62.85	2,574	8,014	
59.73	2,574	4,074	62.91	2,574	8,014	
59.79	2,574	4,186	62.97	2,574	8,014	
59.85	2,574	4,298	63.03	2,574	8,014	
59.91	2,574	4,410	63.09	2,574	8,014	
59.97	2,574	4,522	63.15	2,574	8,014	
60.03	2,574	4,634	63.21	2,574	8,014	
60.09	2,574	4,746	63.27	2,574	8,014	
60.15	2,574	4,858	63.33	2,574	8,014	
60.21	2,574	4,969	63.39	2,574	8,014	
60.27	2,574	5,081	63.45	2,574	8,014	
60.33	2,574	5,193	63.51	2,574	8,014	
60.39	2,574	5,304	63.57	2,574	8,014	
60.45	2,574	5,416	63.63	2,574	8,014	

Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
63.69	2,574	8,014	66.87	2,574	8,014
63.75	2,574	8,014	66.93	2,574	8,014
63.81	2,574	8,014	66.99	2,574	8,014
63.87	2,574	8,014	67.05	2,574	8,014
63.93	2,574	8,014	67.11	2,574	8,014
63.99	2,574	8,014	67.17	2,574	8,014
64.05	2,574	8,014	67.23	2,574	8,014
64.11	2,574	8,014	67.29	2,574	8,014
64.17	2,574	8,014	67.35	2,574	8,014
64.23	2,574	8,014	67.41	2,574	8,014
64.29	2,574	8,014	67.47	2,574	8,014
64.35	2,574	8,014	67.53	2,574	8,014
64.41	2,574	8,014	67.59	2,574	8,014
64.47	2,574	8,014	67.65	2,574	8,014
64.53	2,574	8,014	67.71	2,574	8,014
64.59	2,574	8,014	67.77	2,574	8,014
64.65	2,574	8,014	67.83	2,574	8,014
64.71	2,574	8,014	67.89	2,574	8,014
64.77	2,574	8,014	67.95	2,574	8,014
64.83	2,574	8,014	68.01	2,574	8,014
64.89	2,574	8,014	68.07	2,574	8,014
64.95	2,574	8,014	68.13	2,574	8,014
65.01	2,574	8,014	68.19	2,574	8,014
65.07	2,574	8,014	68.25	2,574	8,014
65.13	2,574	8,014	68.31	2,574	8,014
65.19	2,574	8,014	68.37	2,574	8,014
65.25	2,574	8,014	68.43	2,574	8,014
65.31	2,574	8,014	68.49	2,574	8,014
65.37	2,574	8,014	68.55	2,574	8,014
65.43	2,574	8,014	68.61	2,574	8,014
65.49	2,574	8,014	68.67	2,574	8,014
65.55	2,574	8,014	68.73	2,574	8,014
65.61	2,574	8,014	68.79	2,574	8,014
65.67	2,574	8,014	68.85	2,574	8,014
65.73	2,574	8,014	68.91	2,574	8,014
65.79	2,574	8,014	68.97	2,574	8,014
65.85	2,574	8,014	69.03	2,574	8,014
65.91	2,574	8,014	69.09	2,574	8,014
65.97	2,574	8,014	69.15	2,574	8,014
66.03	2,574	8,014	69.21	2,574	8,014
66.09	2,574	8,014	69.27	2,574	8,014
66.15	2,574	8,014	69.33	2,574	8,014
66.21	2,574	8,014	69.39	2,574	8,014
66.27	2,574	8,014	69.45	2,574	8,014
66.33	2,574	8,014	69.51	2,574	8,014
66.39	2,574	8,014	69.57	2,574	8,014
66.45	2,574	8,014	69.63	2,574	8,014
66.51	2,574	8,014	69.69	2,574	8,014
66.57	2,574	8,014	69.75	2,574	8,014
66.63	2,574	8,014	69.81	2,574	8,014
66.69	2,574	8,014	69.87	2,574	8,014
66.75	2,574	8,014	69.93	2,574	8,014
66.81	2,574	8,014	69.99	2,574	8,014
00.01	2,517	0,017	I """	_,-,- , .	-,

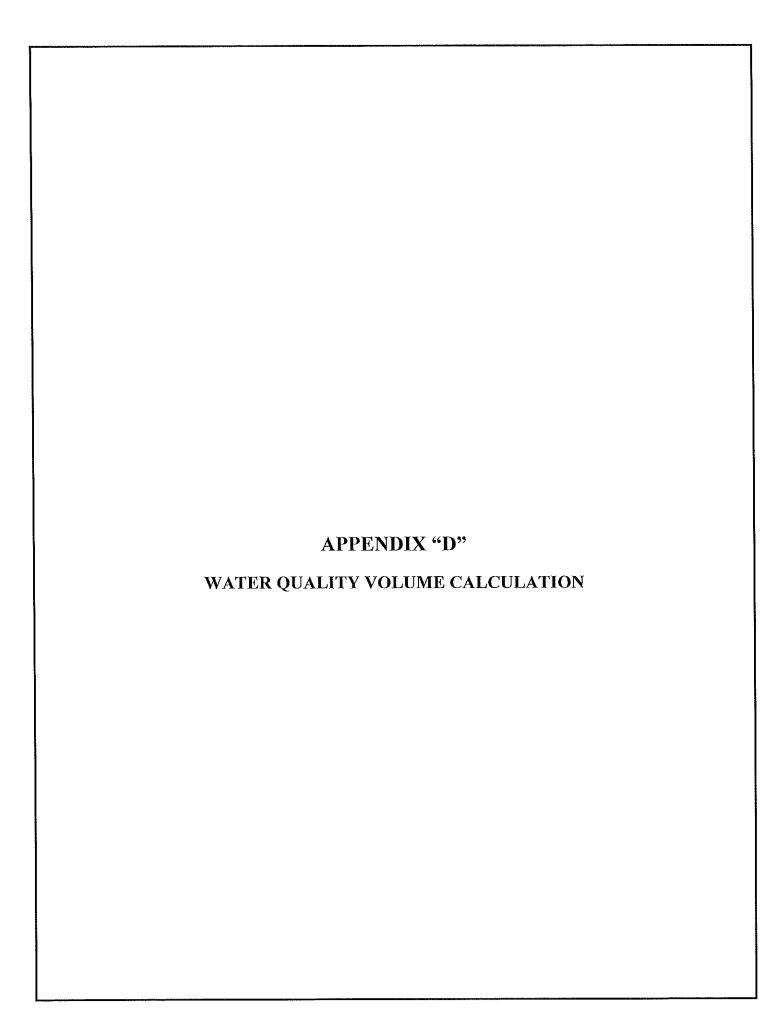
Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
70.05	2,574	8,014	73.23	2,574	8,014
70.11	2,574	8,014	73.29	2,574	8,014
70.17	2,574	8,014	73.35	2,574	8,014
70.23	2,574	8,014	73.41	2,574	8,014
70.29	2,574	8,014	73.47	2,574	8,014
70.35	2,574	8,014	73.53	2,574	8,014
70.41	2,574	8,014	73.59	2,574	8,014
70.47	2,574	8,014	73.65	2,574	8,014
70.53	2,574	8,014	73.71	2,574	8,014
70.59	2,574	8,014	73.77	2,574	8,014
70.65	2,574	8,014	73.83	2,574	8,014
70.71	2,574	8,014	73.89	2,574	8,014
70.77	2,574	8,014	73.95	2,574	8,014
70.83	2,574	8,014	74.01	2,574	8,014
70.89	2,574	8,014	74.07	2,574	8,014
70.95	2,574	8,014	74.13	2,574	8,014
71.01	2,574	8,014	74.19	2,574	8,014
71.07	2,574	8,014	74.25	2,574	8,014
71.13	2,574	8,014	74.31	2,574	8,014
71.19	2,574	8,014	74.37	2,574	8,014
71.25	2,574	8,014	74.43	2,574	8,014
71.31	2,574	8,014	74.49	2,574	8,014
71.37	2,574	8,014	74.55	2,574	8,014
71.43	2,574	8,014	74.61	2,574	8,014
71.49	2,574	8,014	74.67	2,574	8,014
71.55	2,574	8,014	74.73	2,574	8,014
71.61	2,574	8,014	74.79	2,574	8,014
71.67	2,574	8,014	74.85	2,574	8,014
71.73	2,574	8,014	74.91	2,574	8,014
71.79	2,574	8,014	74.97	2,574	8,014
71.85	2,574	8,014	75.03	2,574	8,014 8,014
71.91	2,574	8,014	75.09	2,574 2,574	8,014 8,014
71.97 72.03	2,574	8,014 8,014	75.15 75.21	2,574	8,014 8,014
	2,574 2,574	8,014	75.27	2,574	8,014
72.09 72.15		8,014	75.33	2,574	8,014
72.13	2,574 2,574	8,014	75.39	2,574	8,014
72.27	2,574	8,014	75.45	2,574	8,014
72.33	2,574	8,014	75.51	2,574	8,014
72.39	2,574	8,014	75.57	2,574	8,014
72.45	2,574	8,014	75.63	2,574	8,014
72.51	2,574	8,014	75.69	2,574	8,014
72.57	2,574	8,014	75.75	2,574	8,014
72.63	2,574	8,014	75.81	2,574	8,014
72.69	2,574	8,014	75.87	2,574	8,014
72,75	2,574	8,014	75.93	2,574	8,014
72.81	2,574	8,014	75.99	2,574	8,014
72.87	2,574	8,014	76.05	2,574	8,014
72.93	2,574	8,014	76.11	2,574	8,014
72.99	2,574	8,014	76.17	2,574	8,014
73.05	2,574	8,014	76.23	2,574	8,014
73.11	2,574	8,014	76.29	2,574	8,014
73.17	2,574	8,014	76.35	2,574	8,014
	•		•		

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Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
76.41	2,574	8,014	79.59	2,574	8,014
76.47	2,574	8,014	79.65	2,574	8,014
76.53	2,574	8,014	79.71	2,574	8,014
76.59	2,574	8,014	79.77	2,574	8,014
76.65	2,574	8,014	79.83	2,574	8,014
76.71	2,574	8,014	79.89	2,574	8,014
76.77	2,574	8,014	79.95	2,574	8,014
76.83	2,574	8,014	80.01	2,574	8,014
76.89	2,574	8,014	80.07	2,574	8,014
76.95	2,574	8,014	80.13	2,574	8,014
77.01	2,574	8,014	80.19	2,574	8,014
77.07	2,574	8,014	80.25	2,574	8,014
77.13	2,574	8,014	80.31	2,574	8,014
77.19	2,574	8,014	80.37	2,574	8,014
77.25	2,574	8,014	80.43	2,574	8,014
77.31	2,574	8,014	80,49	2,574	8,014
77.37	2,574	8,014	80.55	2,574	8,014
77.43	2,574	8,014	80.61	2,574	8,014
77.49	2,574	8,014	80.67	2,574	8,014
77.55	2,574	8,014	80.73	2,574	8,014
		8,014	80.79	2,574	8,014
77.61	2,574		80.85	2,574	8,014
77.67	2,574	8,014			
77.73	2,574	8,014	80.91	2,574	8,014
77.79	2,574	8,014	80.97	2,574	8,014
77.85	2,574	8,014	81.03	2,574	8,014
77.91	2,574	8,014	81.09	2,574	8,014
77.97	2,574	8,014	81.15	2,574	8,014
78.03	2,574	8,014	81.21	2,574	8,014
78.09	2,574	8,014	81.27	2,574	8,014
78.15	2,574	8,014	81.33	2,574	8,014
78.21	2,574	8,014	81.39	2,574	8,014
78.27	2,574	8,014	81.45	2,574	8,014
78.33	2,574	8,014	81.51	2,574	8,014
78.39	2,574	8,014	81.57	2,574	8,014
78.45	2,574	8,014	81.63	2,574	8,014
78.51	2,574	8,014	81.69	2,574	8,014
78.57	2,574	8,014	81.75	2,574	8,014
78.63	2,574	8,014	81.81	2,574	8,014
78.69	2,574	8,014	81.87	2,574	8,014
78.75	2,574	8,014	81.93	2,574	8,014
78.81	2,574	8,014	81.99	2,574	8,014
78.87	2,574	8,014	82.05	2,574	8,014
78.93	2,574	8,014	82.11	2,574	8,014
78.99	2,574	8,014	82.17	2,574	8,014
79.05	2,574	8,014	82.23	2,574	8,014
79.11	2,574	8,014	82.29	2,574	8,014
79.17	2,574	8,014	82,35	2,574	8,014
79.23	2,574	8,014	82.41	2,574	8,014
79.29	2,574	8,014	82,47	2,574	8,014
79.35	2,574	8,014	82.53	2,574	8,014
79.41	2,574	8,014	82.59	2,574	8,014
79.47	2,574	8,014	82.65	2,574	8,014
79.53	2,574	8,014	82.71	2,574	8,014
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Printed 3/15/2022

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
82.77	2,574	8,014
82.83	2,574	8,014
82.89	2,574	8,014
82.95	2,574	8,014
83.01	2,574	8,014
83.07	2,574	8,014
83.13	2,574	8,014
83,19	2,574	8,014
83.25	2,574	8,014
83.31	2,574	8,014
83.37	2,574	8,014



Fuller Engineering & Land Surveying, LLC

525 John Street • Second Floor Bridgeport, CT 06604 (203) 333-9465 (203) 336-1769 FAX

#245 Norwich New London Rd. CT Route 32

MONTVILLE, CT

Date:

1/24/22

Revised

3/8/22

Water Quality Volume Calc

Connecticut Stormwater Quality Manual Methodology

Complete

SDU

Drainage

SITE

d By: Checked

By:

Area:

Step 1: Calculate Water Quality Volume, (WQv)

WQv = (1" x R x A) / 12

Where:

R = RvI * %I + RvT * %T + RvF * %F

RvI = Runoff Coefficient for Impervious Cover (SEE MANUAL TABLE 5.5)

%I = Percent of Site in Impervious Cover (Fraction)

RvT = Runoff Coefficient for Lawn %T = Percent of Site in Lawn (Fraction) RvF = Runoff Coefficient for Forest Cover %F = Percent of Site in Forest (Fraction) A = Tributary Drainage Area (Acre)

WQv = Required Water Quality Volume P = 2 Year Frequency Storm (3.4)

	Design Parameters								Water Quality Volume
₽ (in)	A (SF)	RvI	%I	RvT	%Т	RvF	%F	R	(Cu. Ft.)
1.0	79,607.00	0.95	0.40	0.08	0.35	0.05	0.247	0.41584	2758.65

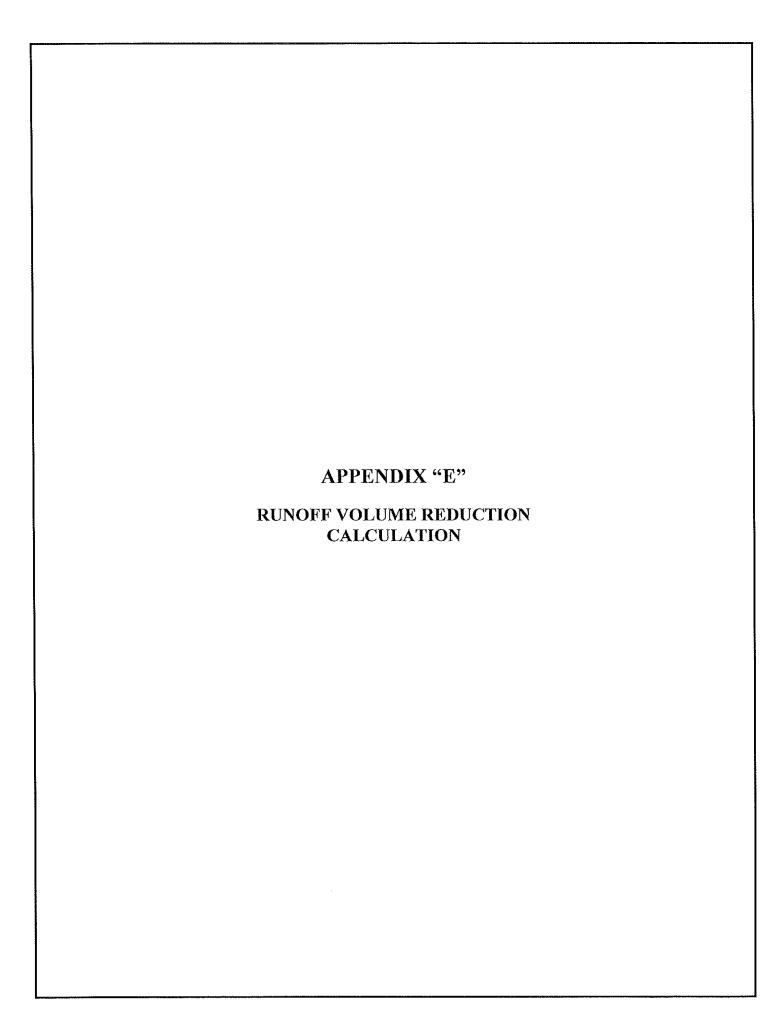
Volume Required to Store On-Site for Cleaning:

2,759 CU. FT.

Inundated Volume provided by the subsurface systems is > 7,000 Cu. Ft.

Vol. provided by the subsurface sys. with inv. set at 61.50' (60 count) = 7,222 Cu. Ft.

Therefore the WQV is Satisfied



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Project: #245 Norwich New London Rd. CT Route 32

MONTVILLE, CT Date: 1/22/22

Revised: 3/8/22

Runoff Volume Reduction Calc

Connecticut Stormwater Quality Manual Methodology Complete d By: SDU

Drainage Site Checked

Area: By:

Step 2: Calculate Runoff Volume Reduction, (RRV)

 $RRV = V_{post} (2yr) - V_{pre} (2yr)$

Where: V_{post} (2yr) = Total Runoff Volume of Post-Construction Site Condition (2 yr, 24 hour storm)

V_{pre} (2yr) = Total Runoff Volume of Pre-Construction Site Condition (2 yr, 24 hour storm)

Design Pa	arameters	Runoff Reduction Volume
Vpost (2yr)	Vpre (2yr)	Kullon Kedaction Volume
	v pre (zyr)	(Cu. Ft.)
10259.00	7613.00	2646.00

Runoff will be infiltrated in proposed underground retention system.

V_{pre} (2yr) = Total Runoff Volume of Pre-Construction Site Condition (2 yr, 24 hour storm) =7,613.0 CF

V_{post} (2yr) = Total Runoff Volume of Post-Construction Site Condition (2 yr, 24 hour storm) (No BMP) =10,259.0 CF

RRV = V_{post} (2yr) - V_{pre} (2yr) = 2,646.0 CF

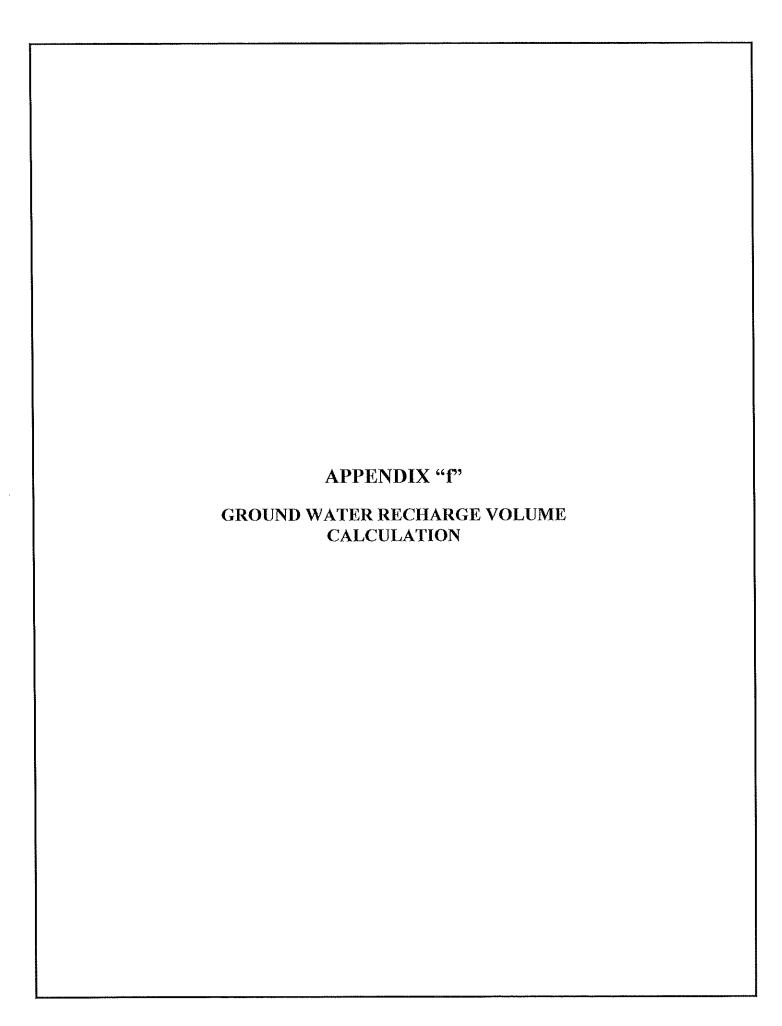
RSV = Proposed Retention Storage Volume * (Total Allowable for system) = 8.010 CF

* Refer to Appendix "C" for Retention Strorage Volume Calculations.

V_{post BMP} = Total Runoff Volume of Post-Construction with BMP's (2 yr, 24 hour storm)

 $V_{post,BMP} = V_{post}(2yr) - RSV$ = 10,259 - 8,010 = 2,249 CF

 $V_{post_BMP} < V_{pre}$ (2yr) Therefore the Runoff Volume Reduction Standard is met.



Fuller Engineering & Land Surveying, LLC

525 John Street • Second Floor Bridgeport, CT 06604 (203) 333-9465 (203) 336-1769 FAX

Project: #245 Norwich New London Rd. CT Route 32

MONTVILLE, CT Date: 1/22/22 Revised: 3/8/22

Runoff Volume Reduction Calc

Connecticut Stormwater Quality Manual Methodology

Complete

d By: SDU

Drainage Site Checked Area: Checked By:

·

Step 2: Calculate Runoff Volume Reduction, (RRV)

 $RRV = V_{post} (2yr) - V_{pre} (2yr)$

Where: V_{post} (2yr) = Total Runoff Volume of Post-Construction Site Condition (2 yr, 24 hour storm)

V_{pre} (2yr) = Total Runoff Volume of Pre-Construction Site Condition (2 yr, 24 hour storm)

Design Pa	arameters	Runoff Reduction Volume		
Vpost (2yr)	Vpre (2yr)	Nation Reduction Volume		
	vpre (zyr)	(Cu. Ft.)		
10259.00	7613.00	2646.00		

Runoff will be infiltrated in proposed underground retention system.

 V_{pre} (2yr) = Total Runoff Volume of Pre-Construction Site Condition (2 yr, 24 hour storm) =7,613.0 CF

V_{post} (2yr) = Total Runoff Volume of Post-Construction Site Condition (2 yr, 24 hour storm)(No BMP) = 10,259.0 CF

RRV = V_{post} (2yr) - V_{pre} (2yr) = 2,646.0 CF

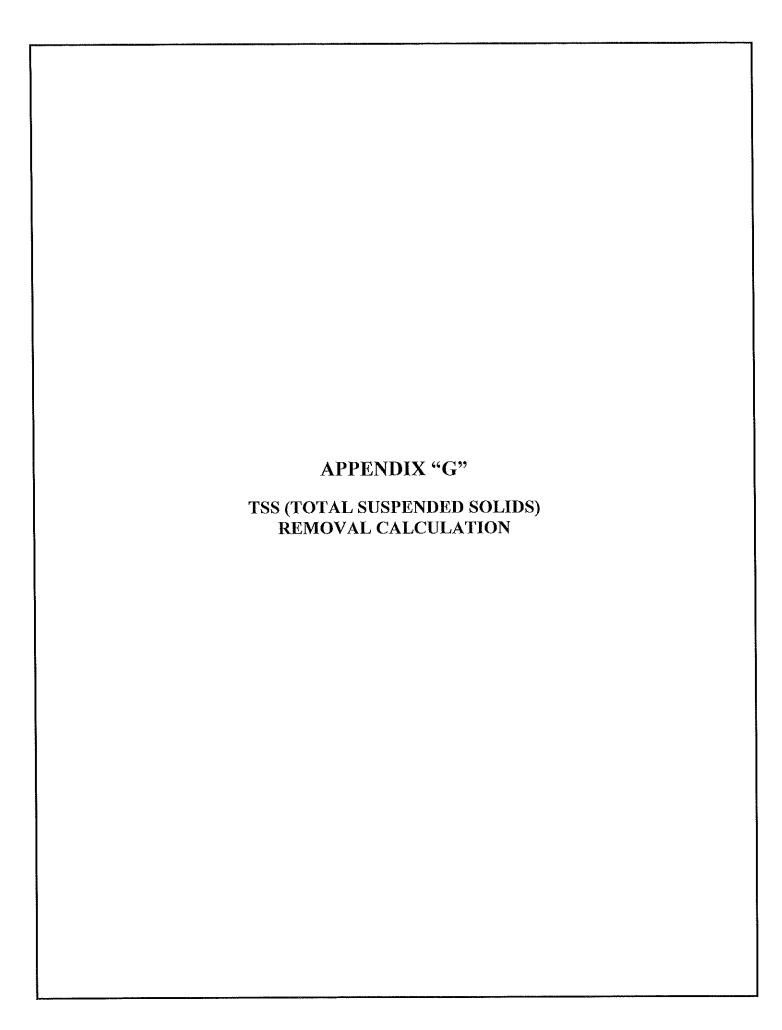
RSV = Proposed Retention Storage Volume * (Total Allowable for system) = 8.010 CF

* Refer to Appendix "C" for Retention Strorage Volume Calculations.

V_{post_BMP} = Total Runoff Volume of Post-Construction with BMP's (2 yr, 24 hour storm)

 $V_{post_BMP} = V_{post} (2yr) - RSV$ = 10,259 - 8,010 = 2,249 CF

 $V_{post_BMP} < V_{pre}$ (2yr) Therefore the Runoff Volume Reduction Standard is met.

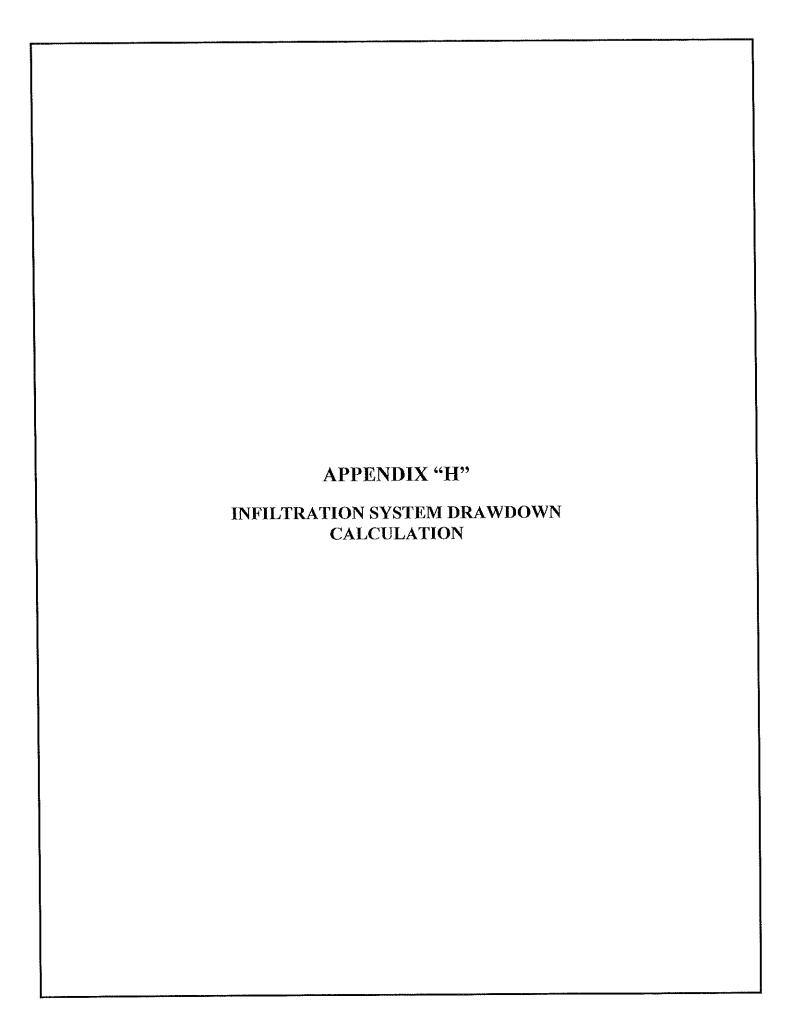


*Equals remaining load from previous BMP (E) which enters the BMP Separate Form Needs to be Completed for Each Outlet or BMP Train Remaining Load (C-D) 0.75 0.08 0.08 0.08 0.08 Pg. 1 of 2 Removed (B*C) Amount 0.00 93% 0.25 99.0 0.00 0.00 Total TSS Removal = C Starting TSS Load* 1.00 0.75 0.08 0.08 0.08 TSS Removal Location: 28 CONCRETE GALLEYS Rate¹ 25% %06 Project: 245 ROUTE 32 Date: 1/24/2022 Prepared By: sou SUBSURFACE STRUCTURE DEEP SUMP CATCH BASIN BMP¹ ⋖

TSS Removal Calculation Worksheet

*Equals remaining load from previous BMP (E) which enters the BMP Separate Form Needs to be Completed for Each Outlet or BMP Train Remaining Load (C-D) 0.01 0.01 0.01 0.01 0.01 Pg. 2 of 2 Removed (B*C) Amount 0.00 %66 0.07 0.00 0.00 0.00 Total TSS Removal = C Starting TSS Load* 0.08 0.01 0.01 0.01 0.01 B TSS Removal Location: 32 CONCRETE GALLEYS Rate¹ %06 25% Project: 245 ROUTE 32 Prepared By: spu
Date: 1/24/2022 SUBSURFACE STRUCTURE DEEP SUMP CATCH BASIN BMP¹ Þ

TSS Removal Calculation Worksheet



FULLER ENGINEERING & LAND SURVEYING, LLC

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DRAWDOWN CALCULATIONS:

Pg. 1 of 2

245 NORWICH-NEW LONDON ROAD STATE ROUTE 32 MONTVILLE, CT

(60) - 4' x 8' x 4' High CONCRETE GALLEY DETENTION/RETENTION SYSTEM

The storage capacity of this retention system is 7,222 cf.

Refer to Appendix "C" for a structure rating table of the system.

SOIL CONDUCTIVITY

RATE = 20 MIN PER IN

3 IN PER HR

SAFETY FACTOR OF 2

RATE = 1.5 IN PER HR

DV = DESIGN VOLUME 7,222 cf

K= INFILTRATION RATE 1.5 in/hr (rate based on Soil Class)
A= BOTTOM AREA 907.68 sf surface area x porosity of stone (122 x 18.6 x 0.4)

Time =
$$\frac{7222}{(1.5)x(907.7)(1/12)}$$

Time = 63.7 hrs

The proposed Concrete Galley System volume will drawdown within 72 Hours.

DRAWDOWN CALCULATION BASED ON THE FOLLOWING:

(Using a conservative Percolation Rate of 20 min./in & Test Pit Data By Others):

TEST HOLE DATA PERFORMED 9/30/14, BY P. LAFAYETTE, P.E.

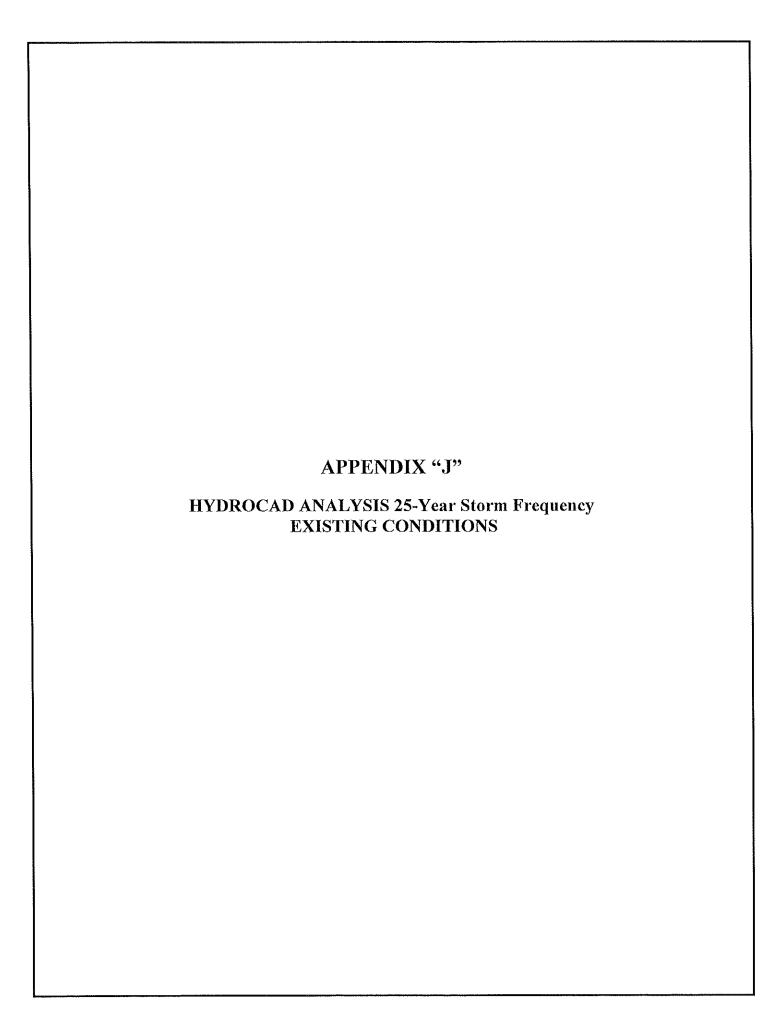
TH-J 0-12" TOPSOIL 12-47" TAN FINE-MED. SAND W/SOME SILT 47-130" MED.-COARSE SAND AND STONES NO MOTTLING, NO WATER, NO LEDGE

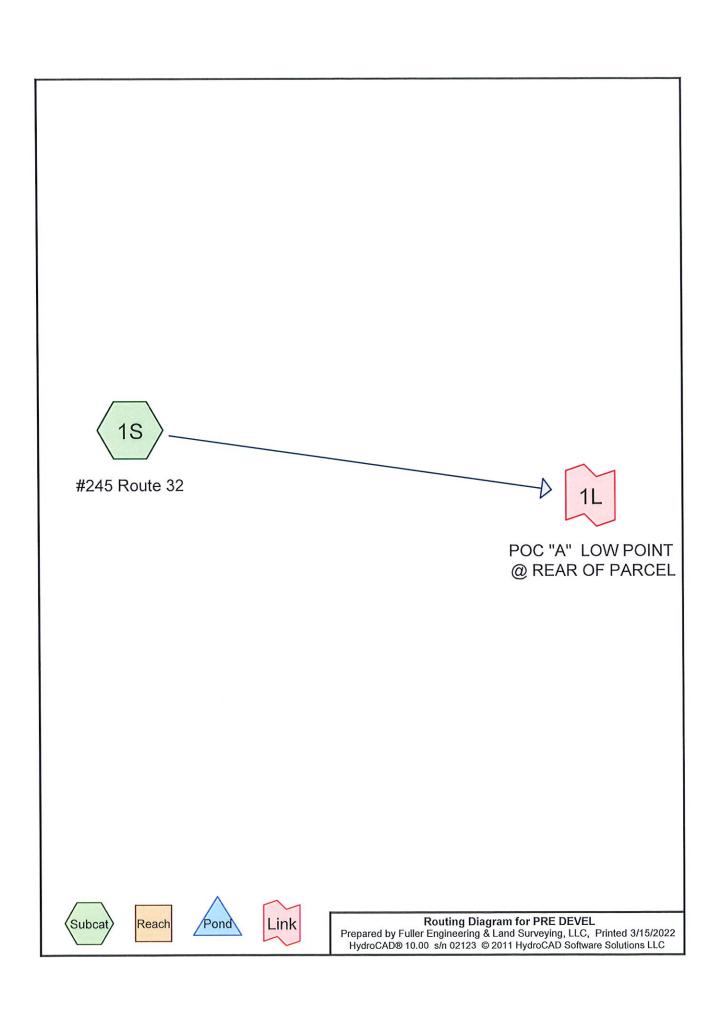
TH=2
0-6" TOPSOIL
6-40" TAN FINE-MED. SAND W/SOME SILT
40-128" MED.-COARSE SAND AND STONES
NO MOTTUNG, NO WATER, NO LEDGE

IH-3
0-4" TOPSOIL
4-32" ORANGE FINE SAND W/SOME SILT & S
32-125" MED.-COARSE SAND AND STONES
NO MOTTLING, NO WATER, NO LEDGE

IH-2
0-10" TOPSOIL
10-52" ORANGE FINE SAND W/SOME SILT & S
52-136" MED.-COARSE SAND AND STONES
NO MOTTLING, NO WATER, NO LEDGE

NOTE: SOIL TESTING DATA PROVIDED BY OTHERS. DEVELOPMENT SOLUTIONS, LLC GRADING, DRAINAGE & UTILITY PLAN - COMMERCIAL/RESIDENTIAL COMPLEX NORWICH-NEW LONDON ROAD (ROUTE 32) MONTVILLE, CONNECTICUT. PREPARED FOR TOMASHE LLC 19 TULSA COURT MONMOUTH JUNCTION, NJ 08852. DATED SEPTEMBER 19, 2014, SCALE: 1" = 20', DRAWING NO. DS - 14 - 545.





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Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
38,866	69	50-75% Grass cover, Fair, HSG B (1S)
38,478	76	Woods/grass comb., Fair, HSG C (1S)
1,661	98	Roofs, HSG B (1S)
22	98	Unconnected pavement, HSG B (1S)
580	98	Unconnected roofs, HSG D (1S)
79,607	73	TOTAL AREA

PRE DEVEL

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Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
40,549	HSG B	18
38,478	HSG C	1S
580	HSG D	18
0	Other	
79,607		TOTAL
		AREA

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Ground Covers (all nodes)

HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover	Subcatchment Numbers
 0	38,866	0	0	0	38,866	50-75% Grass cover, Fair	18
0	22	0	0	0	22	Unconnected pavement	IS
0	1,661	0	0	0	1,661	Roofs	18
0	0	0	580	0	580	Unconnected roofs	1S
0	0	38,478	0	0	38,478	Woods/grass comb., Fair	1S
0	40,549	38,478	580	0	79,607	TOTAL AREA	

#245 Route 32 Montville, CT Type III 24-hr 25-YEAR Rainfall=6.15"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: #245 Route 32

Runoff Area=79,607 sf 2.84% Impervious Runoff Depth>3.20" Flow Length=577' Tc=18.6 min CN=73 Runoff=4.76 cfs 21,240 cf

Link 1L: POC "A" LOW POINT @ REAR OF PARCEL

Inflow=4.76 cfs 21,240 cf Primary=4.76 cfs 21,240 cf

Total Runoff Area = 79,607 sf Runoff Volume = 21,240 cf Average Runoff Depth = 3.20" 97.16% Pervious = 77,344 sf 2.84% Impervious = 2,263 sf

PRE DEVEL

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Summary for Subcatchment 1S: #245 Route 32

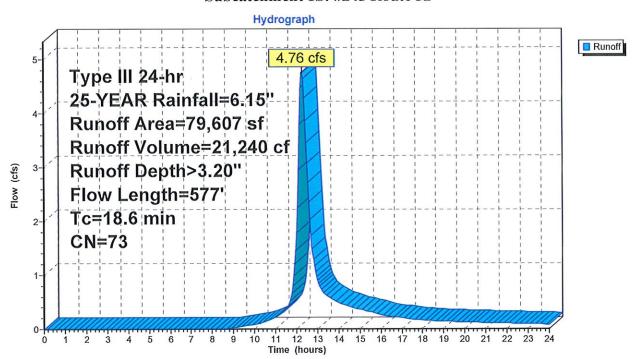
Runoff = 4.76 cfs @ 12.26 hrs, Volume=

21,240 cf, Depth> 3.20"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR Rainfall=6.15"

Aı	rea (sf)	CN	Description						
	1,661	98	Roofs, HSG	Roofs, HSG B					
	22	98	Unconnecte	d pavement	t, HSG B				
	580	98	Unconnecte	d roofs, HS	G D				
	38,478	76	Woods/grass	s comb., Fa	ir, HSG C				
	38,866	69	50-75% Gra	ss cover, Fa	air, HSG B				
	79,607	73	Weighted Average						
	77,344		97.16% Pervious Area						
	2,263		2.84% Impervious Area						
	602		26.60% Und	connected					
Tc	Length	Slope		Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
8.3	477	0.0677	0.96		Lag/CN Method, Overland Flow				
10.3	100	0.1160	0.16		Sheet Flow, Thru the Woods				
					Woods: Light underbrush n= 0.400 P2= 3.40"				
18.6	577	Total							

Subcatchment 1S: #245 Route 32



Hydrograph for Subcatchment 1S: #245 Route 32

Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(cfs)	(hours)	(inches)	(inches)	(cfs)
0.00	0.00	0.00	0.00	13.00	4.61	1.98	0.91
0.25	0.02	0.00	0.00	13.25	4.72	2.06	0.68
0.50	0.03	0.00	0.00	13.50	4.82	2.14	0.60
0.75	0.05	0.00	0.00	13.75	4.91	2.21	0.54
1.00	0.06	0.00	0.00	14.00	4.99	2.27	0.49
1.25	0.08	0.00	0.00	14.25	5.06	2.33	0.45
1.50	0.09	0.00	0.00	14.50	5.13	2.38	0.42
1.75	0.11	0.00	0.00	14.75	5.19	2.43	0.39
2.00	0.12	0.00	0.00	15.00	5.25	2.48	0.37
2.25	0.14	0.00	0.00	15.25	5.31	2.53	0.34
2.50	0.15	0.00	0.00	15,50	5.36	2.57	0.32
2.75	0.17	0.00	0.00	15.75	5.41	2.60	0.29
3.00	0.19	0.00	0.00	16.00	5.45	2.64	0.27
3.25	0.21	0.00	0.00	16.25	5.49	2.67	0.24
3.50	0.23	0.00	0.00	16.50	5.53	2.70	0.23
3.75	0.24	0.00	0.00	16.75	5.56	2.73	0.22
4.00	0.26	0.00	0.00	17.00	5.59	2.75	0.21
4.25	0.28	0.00	0.00	17.25	5.62	2.78	0.20
4.50	0.31	0.00	0.00	17.50	5.65	2.80	0.18
4.75	0.33	0.00	0.00	17.75	5.68	2.83	0.17
5.00	0.35	0.00	0.00	18.00	5.71	2.85	0.16
5.25	0.37	0.00	0.00	18.25	5.73	2.87	0.15
5.50	0.39	0.00	0.00	18.50	5.76	2.89	0.15
5.75	0.42	0.00	0.00	18.75	5.78	2.91	0.14
6.00	0.44	0.00	0.00	19.00	5.80	2.92	0.14
6.25	0.47	0.00	0.00	19.25	5.82	2.94	0.14
6.50	0.50	0.00	0.00	19.50	5.84	2.96	0.13
6.75	0.53	0.00	0.00	19.75	5.87	2.98	0.13
7.00		0.00	0.00	20.00	5.89	2.99	0.13
7.25		0.00	0.00	20.25	5.91	3.01	0.12
7.50		0.00	0.00	20.50	5.92	3.03	0.12 0.12
7.75		0.00	0.00	20.75	5.94 5.96	3.04 3.06	0.12
8.00			0.00	21.00 21.25	5.98 5.98	3.00	0.11
8.25			0.00	21.23		3.09	0.11
8.50			0.00 0.01	21.75		3.10	0.11
8.75			0.01	22.00			0.10
9.00 9.25			0.02	22.25			0.10
9.23			0.05	22.50			0.10
9.30			0.06	22.75			0.10
10.00			0.08	23.00			0.09
10.00			0.11	23.25		3.18	0.09
10.23			0.14	23.50			0.09
10.75			0.17	23.75			0.09
11.00			0.21	24.00			0.08
11.25			0.27		0.12	• • • •	
11.50			0.38				
11.75			0.65				
12.00			1.78				
12.25			4.75				
12.50			3.09				
12.75			1.49				

PRE DEVEL

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Summary for Link 1L: POC "A" LOW POINT @ REAR OF PARCEL

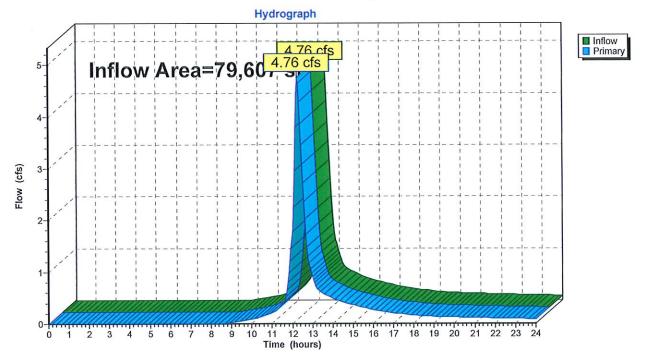
Inflow Area = 79,607 sf, 2.84% Impervious, Inflow Depth > 3.20" for 25-YEAR event

Inflow = 4.76 cfs @ 12.26 hrs, Volume= 21,240 cf

Primary = 4.76 cfs @ 12.26 hrs, Volume= 21,240 cf, Atten= 0%, Lag= 0.0 min

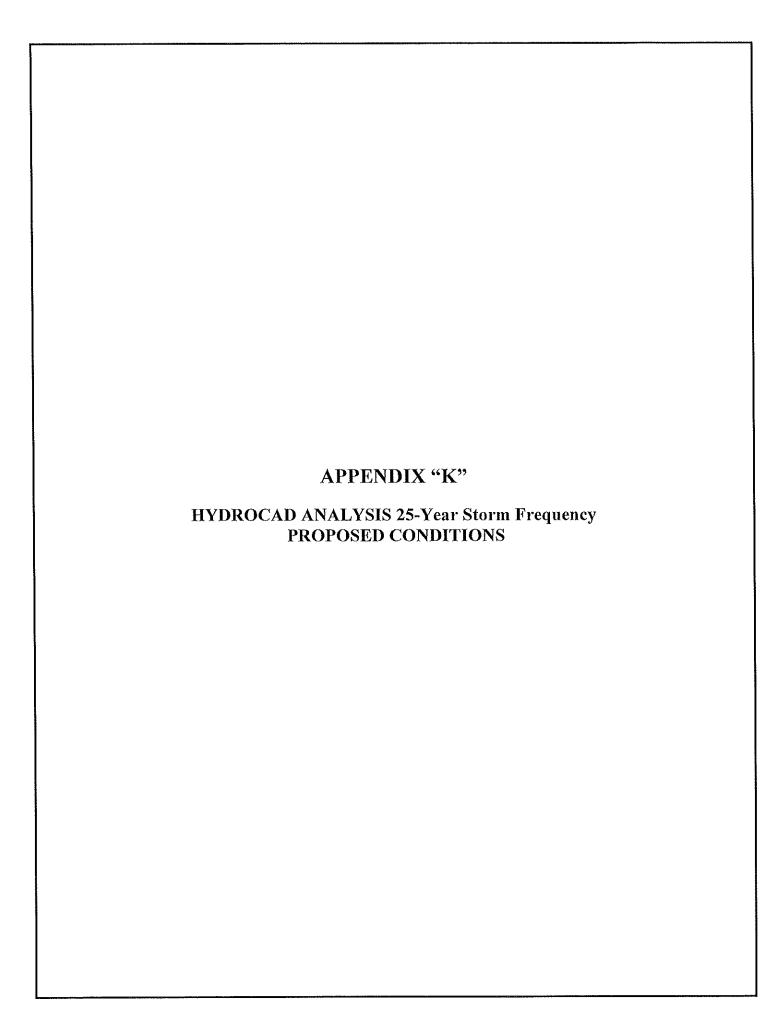
Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

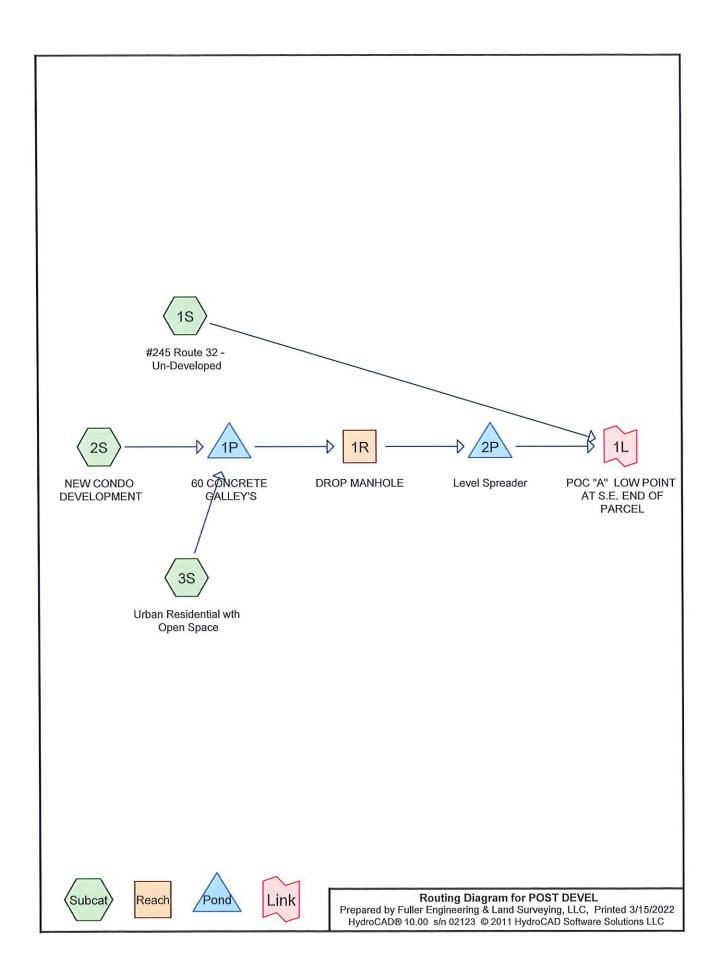
Link 1L: POC "A" LOW POINT @ REAR OF PARCEL



Hydrograph for Link 1L: POC "A" LOW POINT @ REAR OF PARCEL

Time	Inflow	Elevation	Primary	Time	Inflow	Elevation	Primary
(hours)	(cfs)	(fcet)	(cfs)	(hours)	(cfs)	(feet)	(cfs)
0.00	0.00	0.00	0.00	13.00	0.91	0.00	0.91
0.25	0.00	0.00	0.00	13.25	0.68	0.00	0.68
0.50	0.00	0.00	0.00	13.50	0.60	0.00	0.60
0.75	0.00	0.00	0.00	13.75	0.54	0.00	0.54
1.00	0.00	0.00	0.00	14.00	0.49	0.00	0.49
1.25	0.00	0.00	0.00	14.25	0.45	0.00	0.45
1.50	0.00	0.00	0.00	14.50	0.42	0.00	0.42
1.75	0.00	0.00	0.00	14.75	0.39	0.00	0.39
2.00	0.00	0.00	0.00	15.00	0.37	0.00	0.37
2.25	0.00	0.00	0.00	15.25	0.34	0.00	0.34
2.50	0.00	0.00	0.00	15.50	0.32	0.00	0.32
2.75	0.00	0.00	0.00	15.75	0.29	0.00	0.29
3.00	0.00	0.00	0.00	16.00	0.27	0.00	0.27
3.25	0.00	0.00	0.00	16.25	0.24	0.00	0.24
3.50	0.00	0.00	0.00	16.50	0.23	0.00	0.23
3.75	0.00	0.00	0.00	16.75	0.22	0.00	0.22
4.00	0.00	0.00	0.00	17.00	0.21	0.00	0.21
4.25	0.00	0.00	0.00	17.25	0.20	0.00	0.20
4.50	0.00	0.00	0.00	17.50	0.18	0.00	0.18
4.75	0.00	0.00	0.00	17.75	0.17	0.00	0.17
5.00	0.00	0.00	0.00	18.00	0.16	0.00	0.16
5.25	0.00	0.00	0.00	18.25	0.15	0.00	0.15
5.50	0.00	0.00	0.00	18.50	0.15	0.00	0.15
5.75	0.00	0.00	0.00	18.75	0.14	0.00	0.14
6.00	0.00	0.00	0.00	19.00	0.14	0.00	0.14
6.25	0.00	0.00	0.00	19.25	0.14	0.00	0.14
6.50	0.00	0.00	0.00	19.50	0.13	0.00	0.13
6.75	0.00	0.00	0.00	19.75	0.13	0.00	0.13
7.00	0.00	0.00	0.00	20.00	0.13	0.00	0.13
7.25	0.00	0.00	0.00	20.25	0.12	0.00	0.12
7.50	0.00	0.00	0.00	20.50	0.12	0.00	0.12
7.75	0.00	0.00	0.00	20.75	0.12	0.00	0.12
8.00	0.00	0.00	0.00	21.00	0.11	0.00	0.11
8.25	0.00	0.00	0.00	21.25	0.11	0.00	0.11
8.50	0.00	0.00	0.00	21.50	0.11	0.00	0.11
8.75	0.01	0.00	0.01	21.75	0.11	0.00	0.11
9.00	0.02		0.02	22.00	0.10	0.00	0.10
9.25	0.03	0.00	0.03	22.25	0.10	0.00	0.10
9.50	0.05		0.05	22.50	0.10	0.00	0.10
9.75	0.06		0.06	22.75	0.10	0.00	0.10
10.00	0.08		0.08	23.00	0.09	0.00	0.09
10.25	0.11		0.11	23.25	0.09	0.00	0.09
10.50	0.14		0.14	23.50	0.09	0.00	0.09
10.75	0.17		0.17	23.75	0.09	0.00	0.09
11.00	0.21		0.21	24.00	0.08	0.00	0.08
11.25	0.27		0.27				·
11.50	0.38		0.38				
11.75	0.65		0.65				
12.00	1.78		1.78				
12.25	4.75		4.75				
12.50	3.09		3.09				
12.75	1.49		1.49				





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Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
19,658	65	Brush, Good, HSG C (1S)
6,310	69	50-75% Grass cover, Fair, HSG B (3S)
12,016	81	1/3 acre lots, 30% imp, HSG C (2S)
21,238	98	Paved parking, HSG C (3S)
20,385	98	Roofs, HSG B (2S)
79,607	85	TOTAL AREA

POST DEVEL

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Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
26,695	HSG B	2S, 3S
52,912	HSG C	1S, 2S, 3S
0	HSG D	
0	Other	
79,607		TOTAL
		AREA

POST DEVEL

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Ground Covers (all nodes)

HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover	Subcatchment Numbers
0	6,310	0	0	0	6,310	50-75% Grass cover, Fair	3S
0	0	21,238	0	0	21,238	Paved parking	3S
0	20,385	0	0	0	20,385	Roofs	2S
0	0	12,016	0	0	12,016	1/3 acre lots, 30% imp	2S
0	0	19,658	0	0	19,658	Brush, Good	1S
0	26,695	52,912	0	0	79,607	TOTAL AREA	

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: #245 Route 32 - Un-Developed Flow Length=120' Runoff Area=19,658 sf 0.00% Impervious Runoff Depth>2.44" Slope=0.1080 '/' Tc=29.3 min CN=65 Runoff=0.73 cfs 4,004 cf

Subcatchment 2S: NEW CONDO DEVELOPMENT Runoff Area=32,401 sf 74.04% Impervious Runoff Depth>5.19" Flow Length=668' Slope=0.0750' Tc=29.3 min CN=92 Runoff=2.46 cfs 14,025 cf

Subcatchment 3S: Urban Residential wth Open Runoff Area=27,548 sf 77.09% Impervious Runoff Depth>5.08"

Tc=29.3 min CN=91 Runoff=2.06 cfs 11,665 cf

Reach 1R: DROP MANHOLE

Avg. Flow Depth=0.02' Max Vel=99.87 fps Inflow=3.82 cfs 7,342 cf

n=0.013 L=12.0' S=0.7633 '/' Capacity=2,269.48 cfs Outflow=3.82 cfs 7,342 cf

Pond 1P: 60 CONCRETE GALLEY'S

Peak Elev=66.76' Storage=8,014 cf Inflow=4.52 cfs 25,690 cf

Discarded=0.28 cfs 14,683 cf Primary=3.82 cfs 7,342 cf Outflow=4.10 cfs 22,025 cf

Pond 2P: Level Spreader

Peak Elev=53.55' Storage=209 cf Inflow=3.82 cfs 7,342 cf

Discarded=0.00 cfs 0 cf Primary=3.87 cfs 7,145 cf Outflow=3.87 cfs 7,145 cf

Link 1L: POC "A" LOW POINT AT S.E. END OF PARCEL

Inflow=4.52 cfs 11,149 cf
Primary=4.52 cfs 11,149 cf

Total Runoff Area = 79,607 sf Runoff Volume = 29,694 cf Average Runoff Depth = 4.48" 43.19% Pervious = 34,379 sf 56.81% Impervious = 45,228 sf

POST DEVEL

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Summary for Subcatchment 1S: #245 Route 32 - Un-Developed

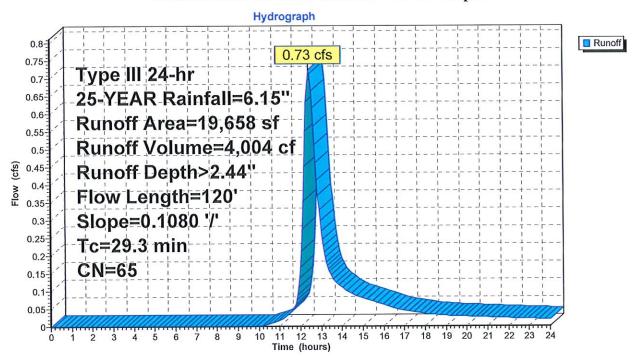
Runoff = 0.73 cfs @ 12.43 hrs, Volume=

4,004 cf, Depth> 2.44"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR Rainfall=6.15"

-	A	rea (sf)	CN	Description		
		19,658	65	Brush, Good	l, HSG C	
19,658 100.00% Pervious Area					rvious Area	
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
•	2.7	120	0.1080	000000000000000000000000000000000000000	` '	Lag/CN Method, Overland Flow
192	26.6	7 44 7 98 50				Direct Entry, HydroStatic Seepage from Wall
10.5	29.3	120	Total			

Subcatchment 1S: #245 Route 32 - Un-Developed



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Hydrograph for Subcatchment 1S: #245 Route 32 - Un-Developed

Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(cfs)	(hours)	(inches)	(inches)	(cfs)
0.00	0.00	0.00	0.00	13.00	4.61	1.40	0.27
0.25	0.02	0.00	0.00	13.25	4.72	1,47	0.18
0.50	0.03	0.00	0.00	13.50	4.82	1.53	0.14
0.75	0.05	0.00	0.00	13.75	4.91	1.59	0.12
1,00	0.06	0.00	0.00	14.00	4.99	1.65	0.11
1.25	80,0	0.00	0.00	14,25	5.06	1.69	0.10
1.50	0.09	0.00	0.00	14.50	5.13	1.74	0.09
1.75	0.11	0.00	0.00	14.75	5.19	1.78	0.09
2.00	0.12	0.00	0.00	15.00	5.25	1.82	0.08
2,25	0.14	0.00	0.00	15.25	5.31	1.86	0.08
2.50	0.15	0.00	0.00	15.50	5.36	1.90	0.07
2.75	0.17	0.00	0.00	15.75	5.41	1.93	0.07
3.00	0.19	0.00	0.00	16.00	5.45	1.96	0.06
3.25	0.21	0.00	0.00	16.25	5.49	1.99	0.06
3.50	0.23	0.00	0.00	16.50	5,53	2.01	0.05
3.75	0.24	0.00	0.00	16.75	5.56	2.04	0.05
4.00	0.26	0.00	0.00	17.00	5,59	2.06	0.05
4.25	0.28	0.00	0.00	17.25	5.62	2.08	0.04
4.50	0.31	0.00	0.00	17.50	5.65	2.10	0.04
4.75	0.33	0.00	0.00	17.75	5.68	2.12	0.04
5.00	0.35	0.00	0.00	18.00	5.71	2.14	0.04
5.25	0.37	0.00	0.00	18.25	5.73	2.16	0.03
5.50	0.39	0.00	0.00	18.50	5.76	2.17	0.03
5.75	0.42	0.00	0.00	18.75	5.78	2.19	0.03
6.00	0.44	0.00	0.00	19.00	5.80	2.21	0.03
6.25	0.47	0.00	0.00	19.25	5.82	2,22	0.03
6.50	0.50	0.00	0.00	19.50	5.84	2.24	0.03
6.75	0.53	0.00	0.00	19.75	5.87	2.25	0.03
7.00	0.56	0.00	0.00	20.00	5.89	2.27	0.03
7.25	0.59	0.00	0.00	20.25	5.91	2.28	0.03
7.50	0.62	0.00	0.00	20.50	5.92	2.30	0.03
7.75	0.66	0.00	0.00	20.75	5.94	2.31	0.03
8.00	0.70	0.00	0.00	21.00	5.96	2.32	0.03
8.25	0.74	0.00	0.00	21.25	5.98	2,34	0.02
8.50	0.79	0.00	0.00	21.50	6.00	2.35	0.02
8.75	0.84	0.00	0.00	21.75	6.01	2.36	0.02
9.00	0.90	0.00	0.00	22.00	6.03	2.37	0.02
9.25	0.96	0.00	0.00	22.25	6.05	2.39	0.02
9.50	1.02	0.00	0.00	22.50	6.06	2.40	0.02
9.75	1.09	0.00	0.00	22.75	6.08	2.41	0.02
10.00		0.00	0.00	23.00	6.09	2.42	0.02
10.25	1.24	0.00	0.00	23.25	6.11	2.43	0.02
10.50	1.33	10.0	0.01	23.50	6.12		0.02
10.75		0.02	0.01	23.75	6.14		0.02
11.00		0.04	0.02	24.00	6.15	2.46	0.02
11.25		0.06	0.02				
11.50		0.09	0.04				
11.75		0.19	0.06 0.17				
12.00				1			
12.25 12.50			0.55 0.70				
12.30			0.70				
12.73	4.40	1,34	0.40	I			

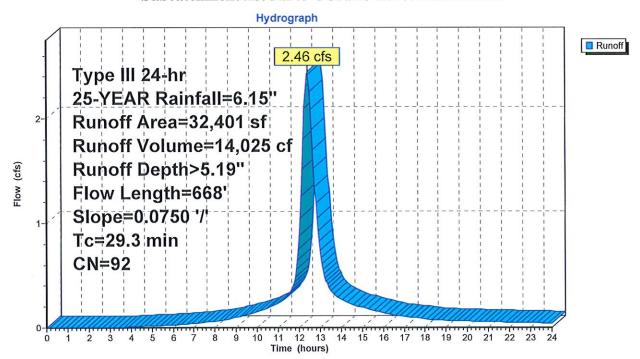
Summary for Subcatchment 2S: NEW CONDO DEVELOPMENT

Runoff = 2.46 cfs @ 12.39 hrs, Volume= 14,025 cf, Depth> 5.19"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR Rainfall=6.15"

	Aı	rea (sf)	CN	Description			
		20,385	98	Roofs, HSG	В		
		12,016	81	1/3 acre lots	, 30% imp,	HSG C	
	32,401 92 Weighted Average						
		8,411					
	23,990 74.04% Impervious Area						
	Tc	Length	Slope		Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	18.5					Direct Entry, DIRECT	
	0.6	456		12.69		Lake or Reservoir, DETENTION	
						Mean Depth= 5.00'	
	10.2	212	0.0750	0.35		Sheet Flow, OverLand Flow	
_						Grass: Short n= 0.150 P2= 3.40"	
	29.3	668	Total				

Subcatchment 2S: NEW CONDO DEVELOPMENT



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Hydrograph for Subcatchment 2S: NEW CONDO DEVELOPMENT

Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(cfs)	(hours)	(inches)		(cfs)
0.00	0.00	0.00	0.00	13.00	4.61	3.71	0.74
0.25	0.02	0.00	0.00	13.25	4.72	3,82	0.48
0.50	0.03	0.00	0.00	13.50	4.82	3.91	0.36
0.75	0.05	0.00	0.00	13.75	4.91	4.00	0.30
1.00	0.06	0.00	0.00	14.00	4.99	4.08	0.27
1.25	0.08	0.00	0.00	14.25	5.06	4.15	0.24
1.50	0.09	0.00	0.00	14.50	5.13	4.22	0.22
1.75	0.11	0.00	0.00	14.75	5.19	4.28	0.21
2.00	0.12	0.00	0.00	15.00	5.25	4.34	0.19
2.25	0.14	0.00	0.00	15.25	5.31	4.39	0.18
2.50	0.15	0.00	0.00	15.50	5.36	4.44	0.17
2.75	0.17	0.00	0.00	15.75	5.41	4.49	0.15
3.00	0.19	0.00	0.00	16.00	5.45	4.53	0.14
3.25	0.21	0.00	0.00	16.25	5.49	4.57	0.13
3.50	0.23	0.00	0.00	16.50	5.53	4.60	0.12
3.75	0.24	0.01	0.00	16.75	5.56	4.64	0.11
4.00	0.26	0.01	0.01	17.00	5.59	4.67	0.11
4.25	0.28	0.01	0.01	17.25	5.62	4.70	0.10
4.50	0.31	0.02	0.01	17.50	5.65	4.73	0.09
4.75	0.33	0.02	10.0	17.75	5.68	4.76	0.09
5.00	0.35	0.03	0.02	18.00	5.71	4.78	0.08
5.25	0.37	0.04	0.02	18.25	5.73	4.81	0.08
5.50	0.39	0.04	0.02	18.50	5.76	4.83	0.07
5.75	0.42	0.05	0.02	18.75	5.78	4.85 4.87	0.07
6.00	0.44	0.06 0.07	0.03 0.03	19.00 19.25	5.80 5.82	4.87	0.07 0.07
6.25	0.47 0.50	0.07	0.03	19.23	5.84	4.90	0.07
6.50 6.75	0.53	0.09	0.03	19.30	5.87	4.94	0.07
7.00	0.56	0.10	0.04	20.00	5.89	4.96	0.06
7.00	0.50	0.12	0.04	20.25	5.91	4.98	0.06
7.50	0.62	0.15	0.05	20.50	5.92	5.00	0.06
7.75	0.66	0.18	0.06	20.75	5.94	5.01	0.06
8.00	0.70	0.20	0.06	21.00	5.96	5.03	0.06
8.25	0.74	0.23	0.07	21.25	5.98	5.05	0.05
8.50	0.79		0.08	21.50	6.00	5.07	0.05
8.75	0.84		0.09	21.75	6.01	5.08	0.05
9.00	0.90		0.10	22.00	6.03	5.10	0.05
9.25	0.96		0.11	22,25	6.05	5.12	0.05
9.50	1.02		0.12	22.50	6.06	5.13	0.05
9.75	1.09	0.47	0.14	22.75	6.08	5.15	0.05
10.00	1.16	0.53	0.15	23.00	6.09	5.16	0.05
10.25	1.24	0.59	0.17	23.25	6.11	5.18	0.04
10.50			0.18	23.50	6.12	5.19	0.04
10.75			0.21	23.75	6.14	5.20	0.04
11.00			0.24	24.00	6.15	5.22	0.04
11.25			0.27				
11.50			0.32				
11.75			0.44				
12.00			0.88				
12.25			2.09				
12.50			2.26				
12.75	4.48	3.59	1.35	I			

POST DEVEL

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Summary for Subcatchment 3S: Urban Residential wth Open Space

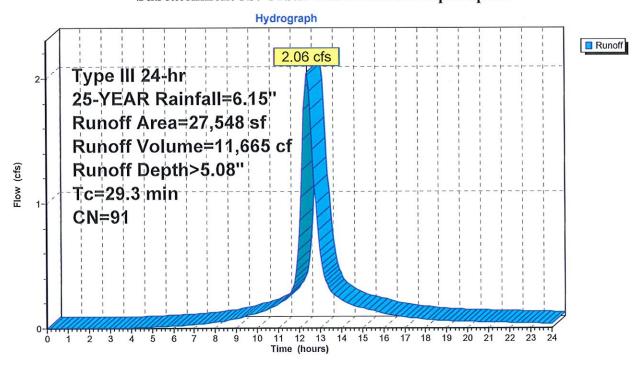
Runoff = 2.06 cfs @ 12.39 hrs, Volume=

11,665 cf, Depth> 5.08"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR Rainfall=6.15"

	A	rea (sf)	CN	Description						
		6,310	69	50-75% Gra	50-75% Grass cover, Fair, HSG B					
	1	21,238	98	Paved parki	ng, HSG C					
		27,548	91	Weighted A	verage					
	6,310 22.91% Pervious Area									
		21,238		77.09% Imp	ervious Are	ea				
	Tc	Length	Slop		Capacity	Description				
((min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
	29.3					Direct Entry, DIRECT				

Subcatchment 3S: Urban Residential wth Open Space



Hydrograph for Subcatchment 3S: Urban Residential wth Open Space

Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(cfs)	(hours)	(inches)	(inches)	(cfs)
0.00	0.00	0.00	0.00	13.00	4.61	3.61	0.62
0.25	0.02	0.00	0.00	13.25	4.72	3.71	0.40
0.50	0.03	0.00	0.00	13.50	4.82	3.81	0.30
0.75	0.05	0.00	0.00	13.75	4.91	3.89	0.26
1.00	0.06	0.00	0.00	14.00	4.99	3.97	0.23
1.25	0.08	0.00	0.00	14.25	5.06	4.04	0.21
1.50	0.09	0.00	0.00	14.50	5.13	4.11	0.19
1.75	0.11	0.00	0.00	14.75	5.19	4.17	0.17
2.00	0.12	0.00	0.00	15.00	5.25	4.23	0.16
2.25	0.14	0.00	0.00	15.25	5.31	4.28	0.15
2.50	0.15	0.00	0.00	15.50	5.36	4.33	0.14
2.75	0.17	0.00	0.00	15.75	5.41	4.38	0.13
3.00	0.19	0.00	0.00	16.00	5.45	4.42	0.12
3.25	0.21	0.00	0.00	16.25	5.49	4.46	0.11
3.50	0.23	0.00	0.00	16.50	5.53	4.49	0.10
3.75	0.24	0.00	0.00	16.75	5.56	4.53	0.09
4.00	0.26	0.00	0.00	17.00	5.59	4.56	0.09
4.25	0.28	0.01	0.00	17.25	5.62	4.59	0.08
4,50	0.31	0.01	0.01	17.50	5.65	4.62	80.0
4.75	0.33	0.01	0.01	17.75	5.68	4.65	0.07
5.00	0.35	0.02	0.01	18.00	5.71	4.67	0.07
5.25	0.37	0.03	0.01	18.25	5.73	4.69	0.07
5.50	0.39	0.03	0.01	18.50	5.76	4.72	0.06
5.75	0.42	0.04	0.02	18.75	5.78	4.74	0.06
6.00	0.44	0.05	0.02	19.00	5.80	4.76	0.06 0.06
6.25	0.47	0.06	0.02	19.25	5.82	4.78	
6.50	0.50	0.07	0.02	19.50	5.84 5.87	4.81 4.83	0.06 0.05
6.75	0.53	0.08	0.03 0.03	19.75 20.00	5.89	4.85	0.05
7.00 7.25	0.56 0.59	$0.10 \\ 0.11$	0.03	20.00	5.91	4.85	0.05
7.23	0.39	0.11	0.03	20.23	5.92	4.88	0.05
7.75	0.62	0.15	0.04	20.75	5.94	4.90	0.05
8.00	0.30	0.13	0.04	21.00	5.96	4.92	0.05
8.25	0.74	0.17	0.05	21.25	5.98	4.94	0.05
8.50	0.79		0.06	21.50	6.00	4.95	0.05
8.75	0.84	0.25	0.07	21.75	6.01	4.97	0.04
9.00	0.90		0.08	22.00	6.03	4.99	0.04
9.25	0.96		0.09	22.25	6.05	5.00	0.04
9.50	1.02		0.10	22.50	6.06	5.02	0.04
9.75	1.09		0.11	22.75	6.08	5.03	0.04
10.00	1.16		0.12	23.00			0.04
10.25			0.13	23.25		5.06	0.04
10.50			0.15	23.50		5.08	0.04
10.75			0.17	23.75	6.14	5.09	0.04
11.00	1.54	0.77	0.19	24.00	6.15	5.10	0.03
11.25			0.22	1			
11.50	1.83		0.26				
11.75			0.36				
12.00			0.73				
12.25			1.75				
12.50			1.90				
12.75	4.48	3.48	1.14				

POST DEVEL

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Summary for Reach 1R: DROP MANHOLE

Inflow Area = 59,949 sf, 75.44% Impervious, Inflow Depth = 1.47" for 25-YEAR event

Inflow = 3.82 cfs @ 12.57 hrs, Volume= 7,342 cf

Outflow = 3.82 cfs @ 12.57 hrs, Volume= 7,342 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Max. Velocity= 99.87 fps, Min. Travel Time= 0.0 min Avg. Velocity = 99.87 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 12.57 hrs

Average Depth at Peak Storage= 0.02'

Bank-Full Depth= 12.00' Flow Area= 19.6 sf, Capacity= 2,269.48 cfs

Custom stage-perimeter table, n= 0.013 Concrete pipe, bends & connections 100 Intermediate values determined by Multi-point interpolation

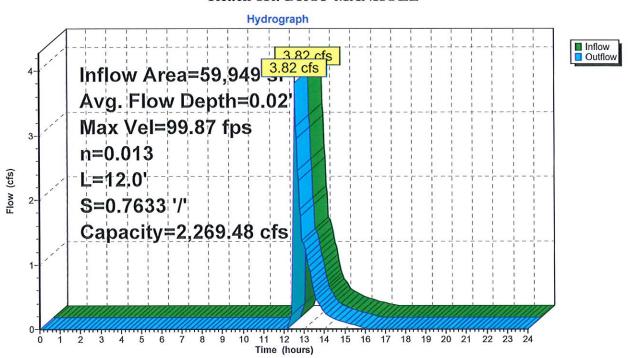
Length= 12.0' Slope= 0.7633 '/'

Inlet Invert= 61.16', Outlet Invert= 52.00'



	Depth	End Area	Perim.	Storage	Discharge
	(feet)	(sq-ft)	(feet)	(cubic-feet)	(cfs)
Ī	0.00	0.0	0.0	0	0.00
	6.00	12.6	12.6	151	1,258.35
	12.00	19.6	15.7	235	2,269.48

Reach 1R: DROP MANHOLE



Reach 1R: DROP MANHOLE

